



Calibration of the Scanning High-resolution Interferometer Sounder (S-HIS) Infrared Spectrometer: Overview (Part 1)

Hank Revercomb and Fred Best

University of Wisconsin-Madison,
Space Science and Engineering Center



2005 Calcon Workshop
Calibration of Airborne Sensor Systems
Utah State, 22 August 2005





TOPICS

1. S-HIS Summary
2. S-HIS Radiometric & Spectral Calibration
3. Tests of High Spectral Resolution Calibration
(including S-HIS comparison to AIRS)
4. The Promise of CrIS for NPOESS



1. S-HIS Summary

UW Scanning HIS: 1998-Present

(HIS: High-resolution Interferometer Sounder, 1985-1998)

Characteristics

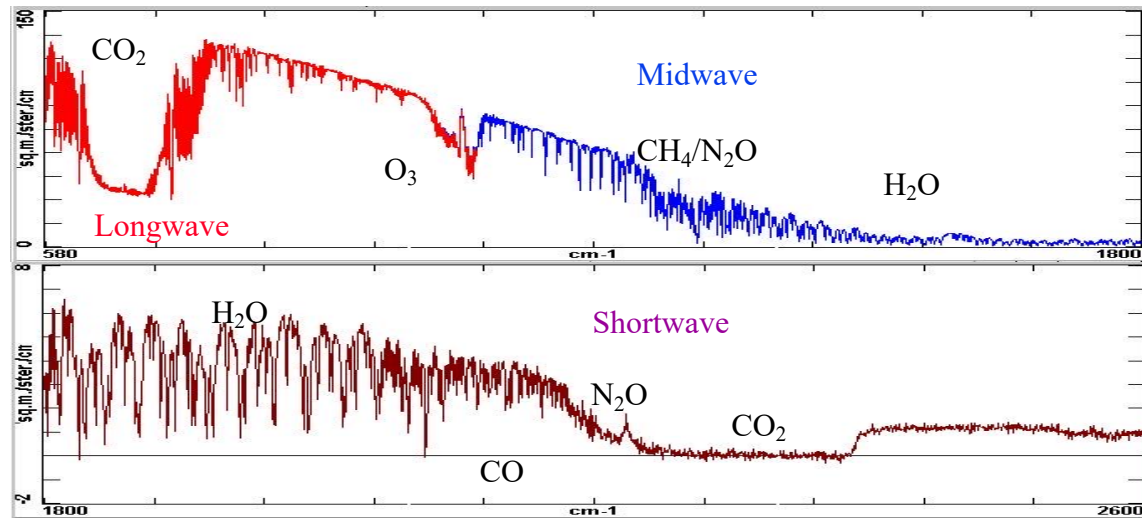
Spectral Coverage: 3-17 microns

Spectral Resolution: 0.5 cm^{-1}

Resolving power: 1000-6000

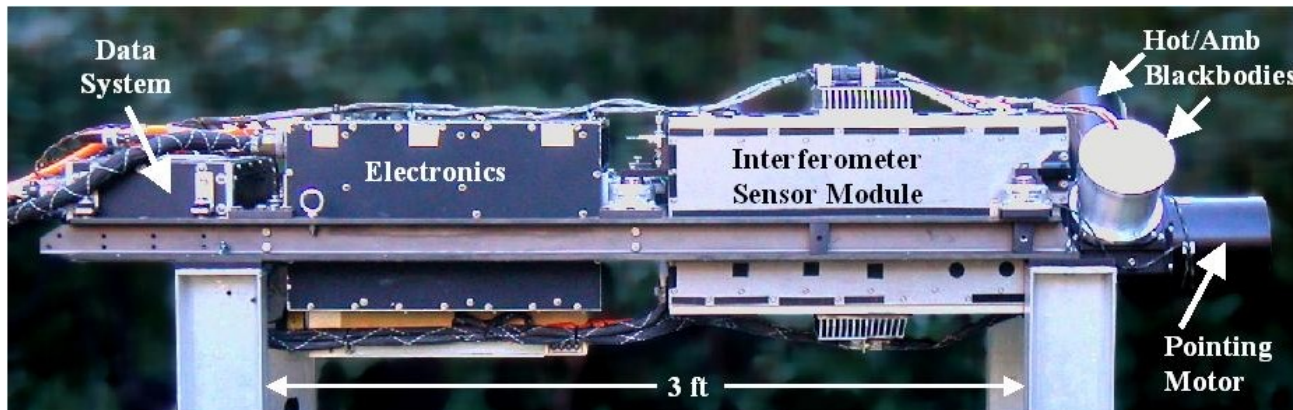
Footprint Diam: 1.5 km @ 15 km

Cross-Track Scan: Programmable including uplooking zenith view



Applications:

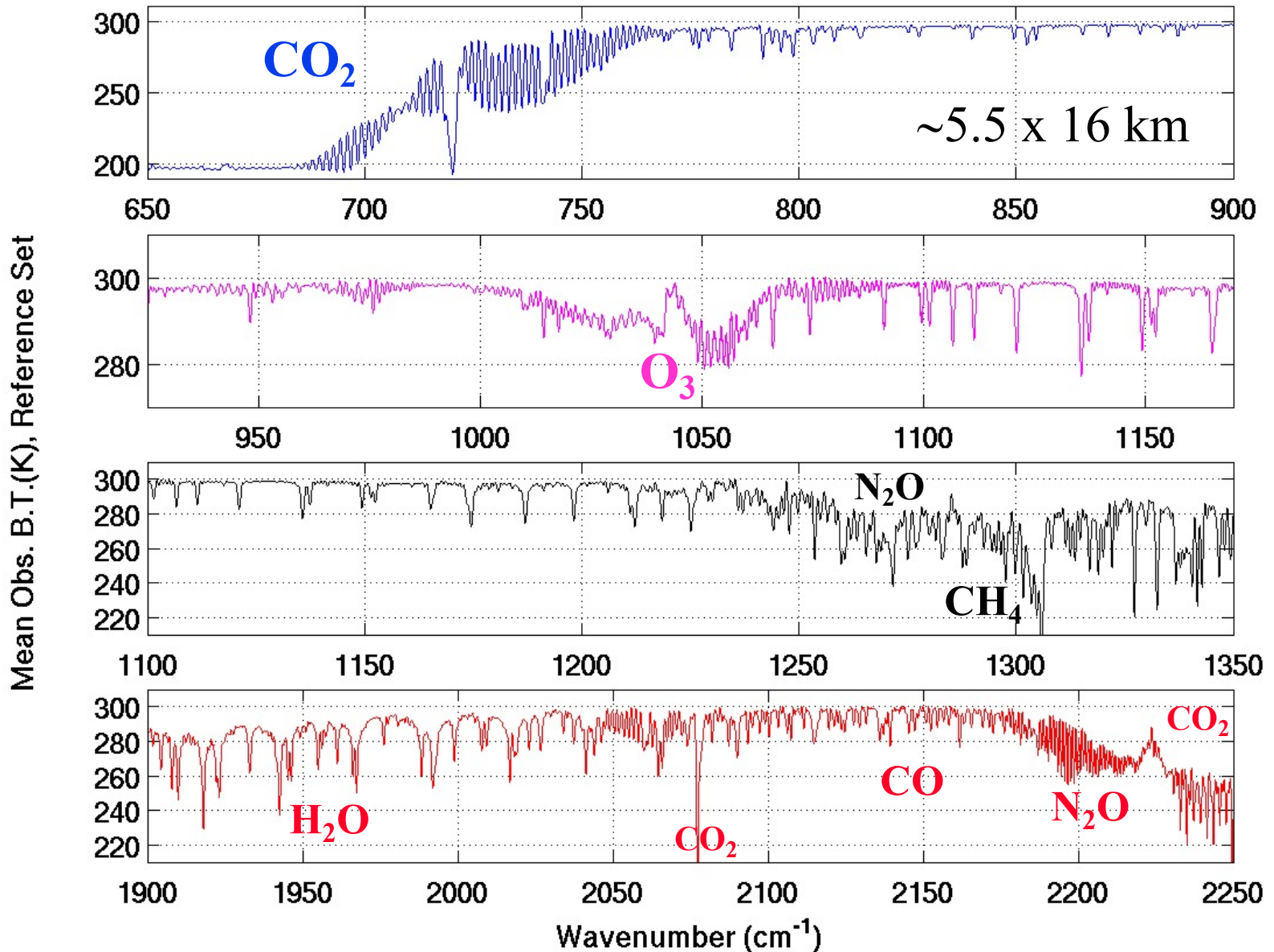
- ◆ Radiances for Radiative Transfer
- ◆ Temp & Water Vapor Retrievals
- ◆ Cloud Radiative Prop.
- ◆ Surface Emissivity & T
- ◆ Trace Gas Retrievals



S-HIS – Tropospheric Emission Spectrometer (TES) Bands

near 31 Oct overpass

SHIS for TES Validation (Bands 2B1, 1B2, 2A1, 1A1), 31 Oct. 2004, 19.273 to 19.298 UTC

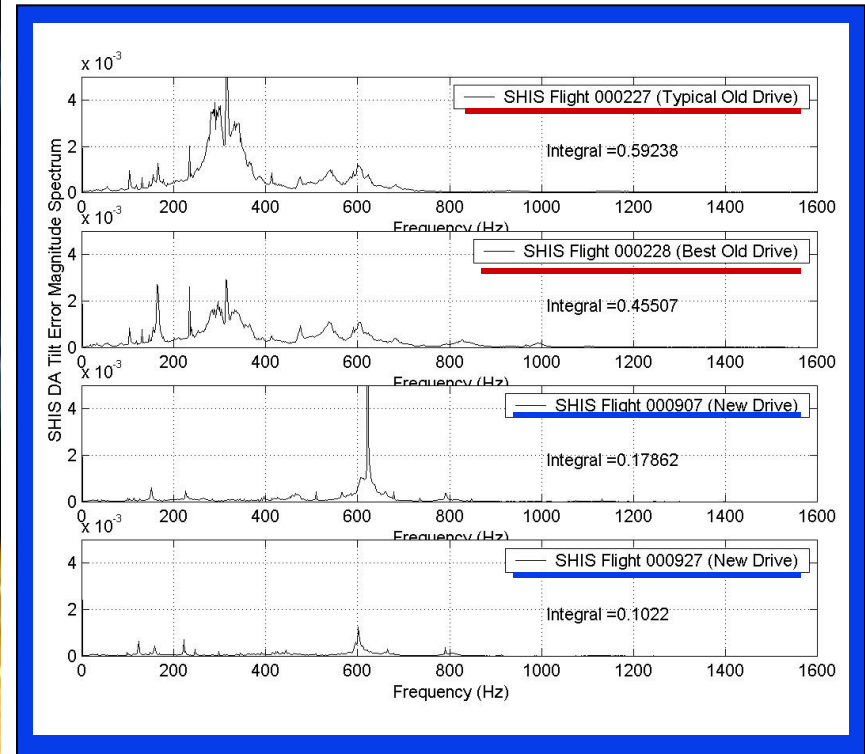


Scanning HIS Interferometer: with Telescope, Collection optics, & Detectors/Cooler



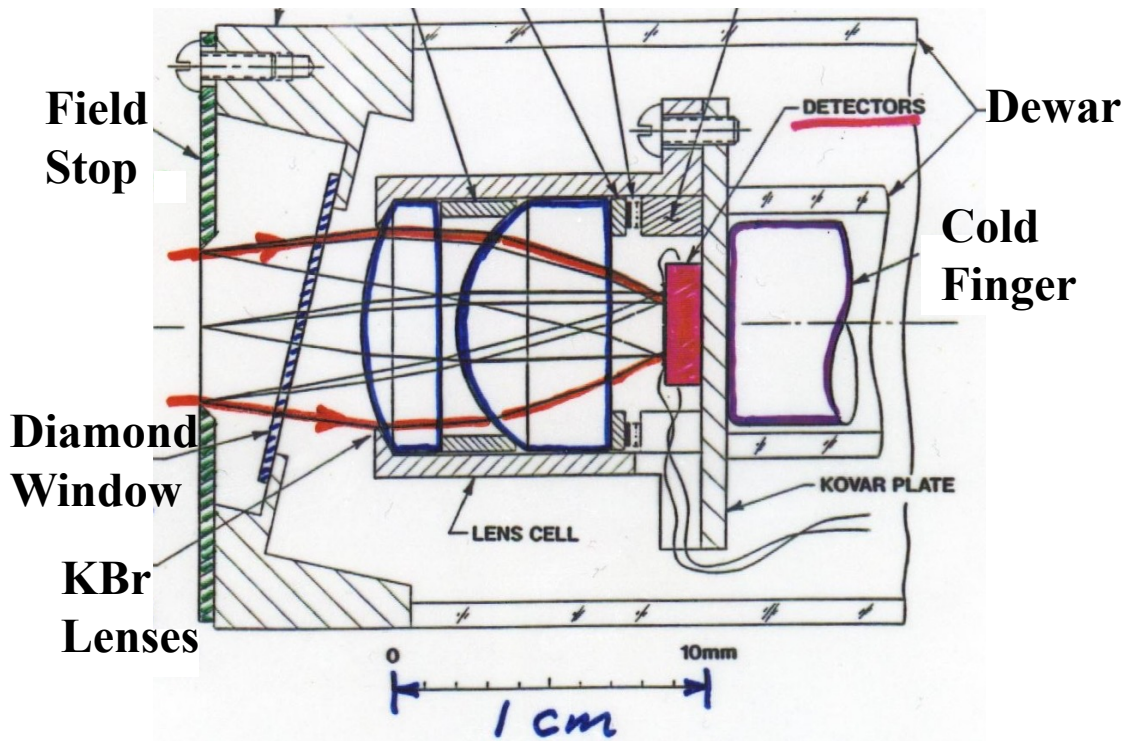
Laser metrology located on bottom of optical bench

S-HIS Linear Bearing Based Michelson Drive

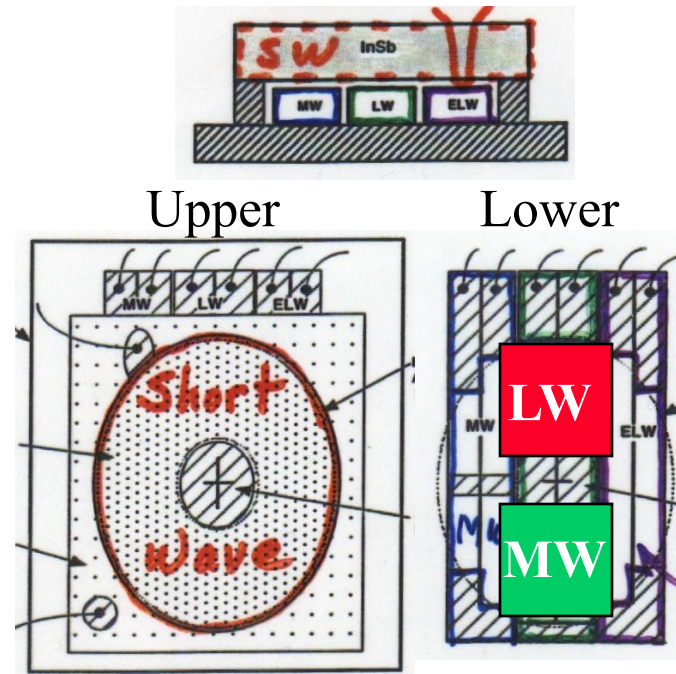


Comparison of Tilt Spectra measured during flight from the **old** and **new** Michelson Drive assemblies as measured by the S-HIS laser based dynamic Alignment system. The new drive eliminates significant tilt dynamic amplitude Below 600 Hz. In addition, the overall tilt magnitude is lower by almost a factor 6 with the new drive.

Scanning HIS Detector/Dewar Configuration



Dewar with tilted diamond window & KBr lenses



Sandwich Detectors:
Shortwave InSb on top
MW & LW below

S-HIS Split Cycle Stirling Cooler

- ◆ Allows vibration isolation
- ◆ Simplifies cooler replacement

Compliant
Transfer Tube
Allows mechanical
decoupling

Compressor



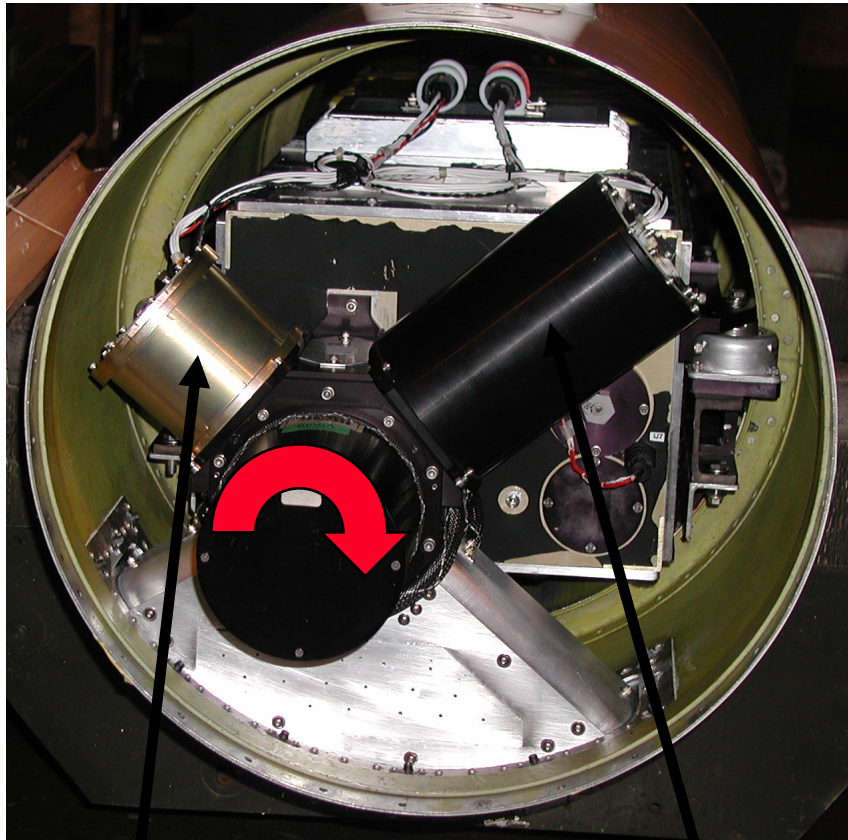
Cooler
Exander

Detector

Litton cooler with dewar

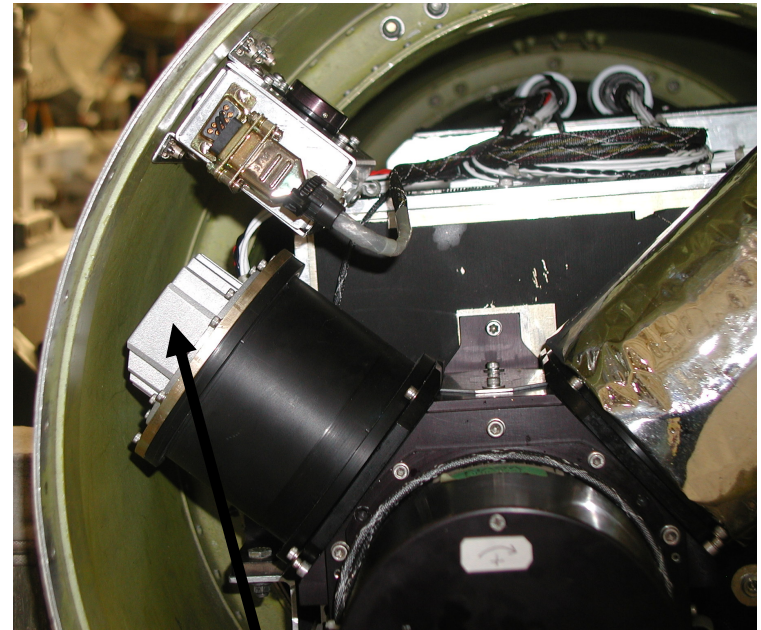
S-HIS In-Flight Calibration

- Hot and Cold onboard BBs viewed every x-track scan (12 sec).



Ambient BB

Hot BB

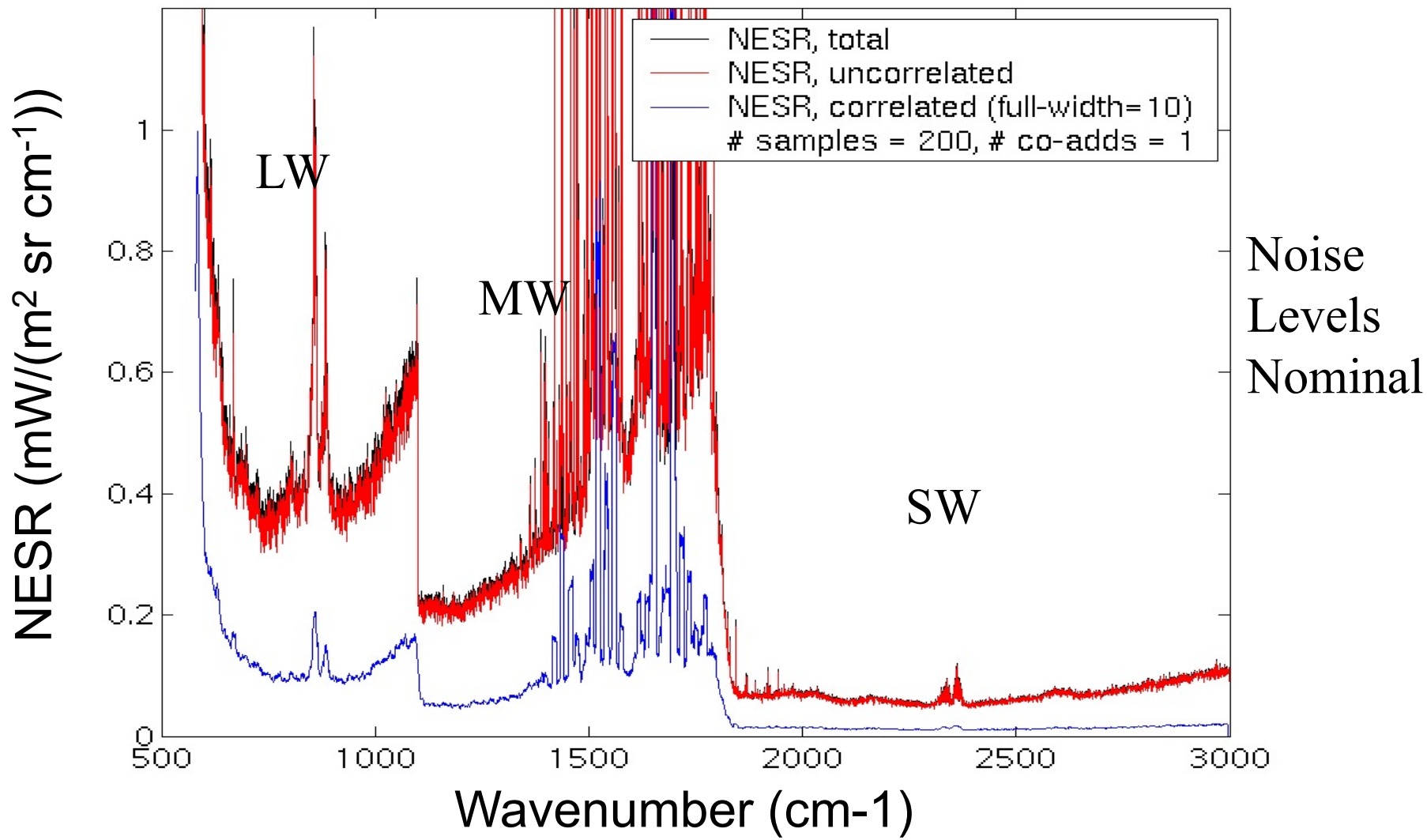


Cooling fins closely couple the Cold Blackbody to the Pod Ambient Air Temperature.

Instrument Characteristics



UW Pre-Mission Cal. Verification



SSEC Scanning HIS on 1st ARM-UAV Mission with Proteus, October 2002



S-HIS scans cross-track downward & looks upward



Aura Validation Expt

AVE, Oct/Nov 2004



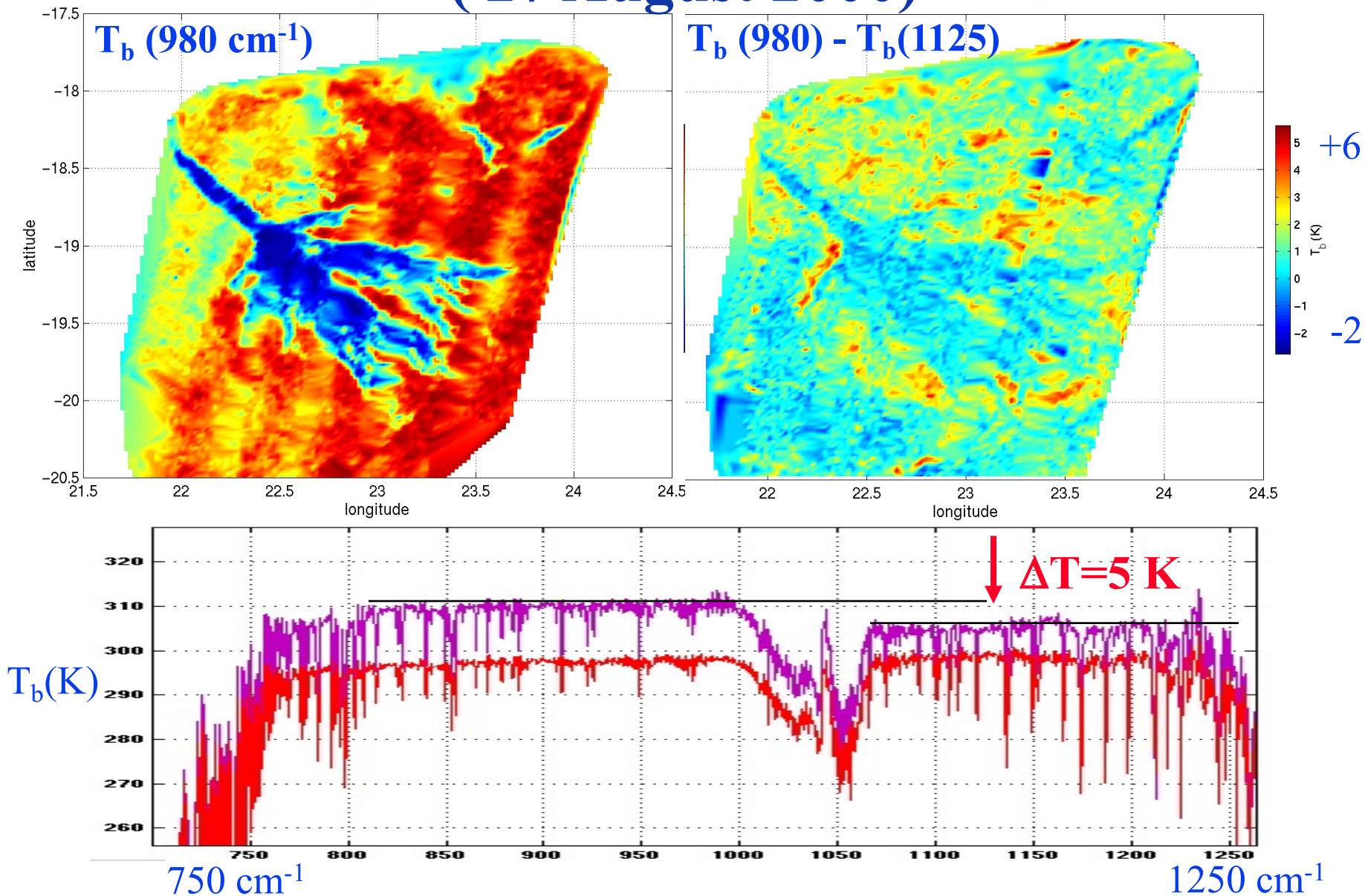
NASA WB57



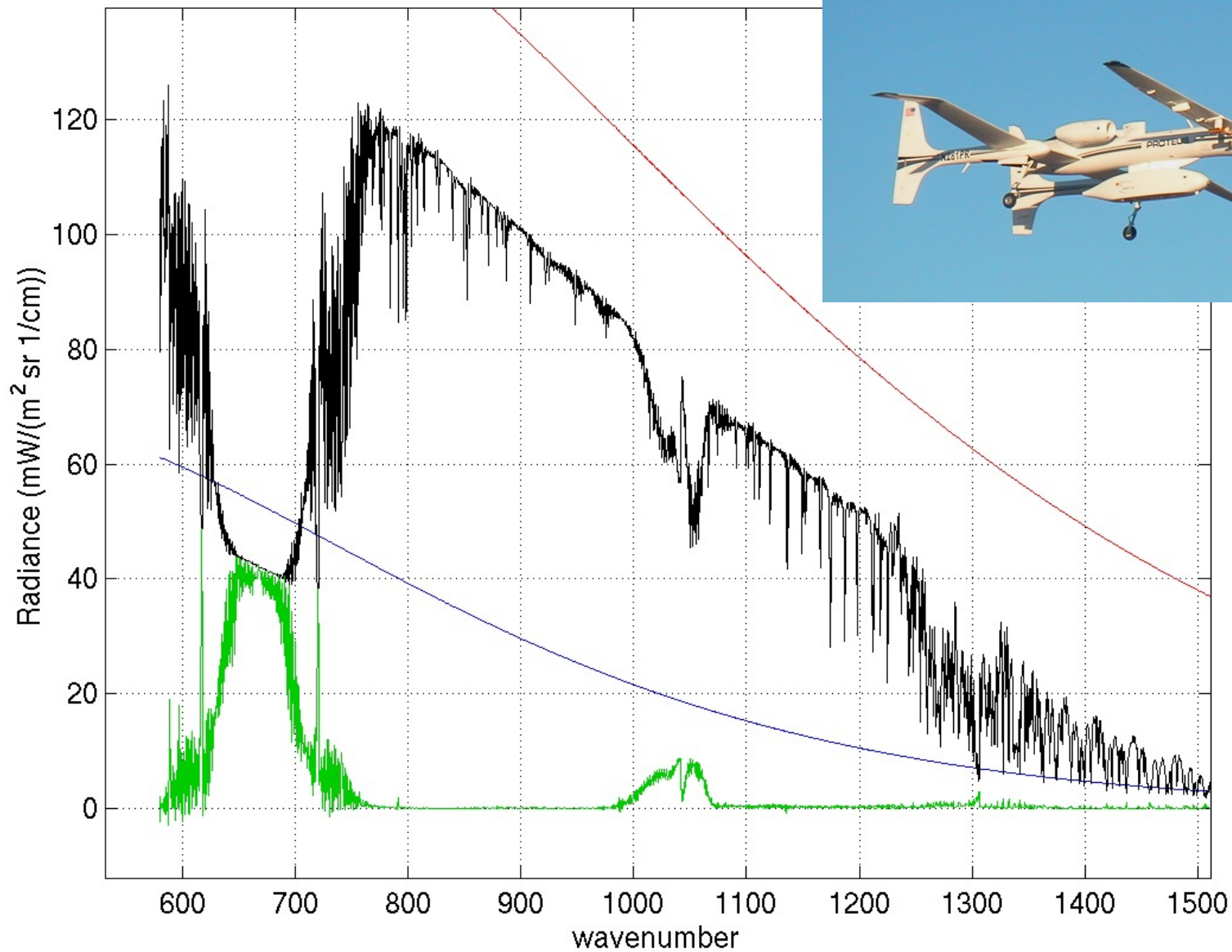
S-HIS
scans cross-
track downward
&
looks upward

Left Wing Pod

Okavanga Delta Surface Emissivity (27 August 2000)



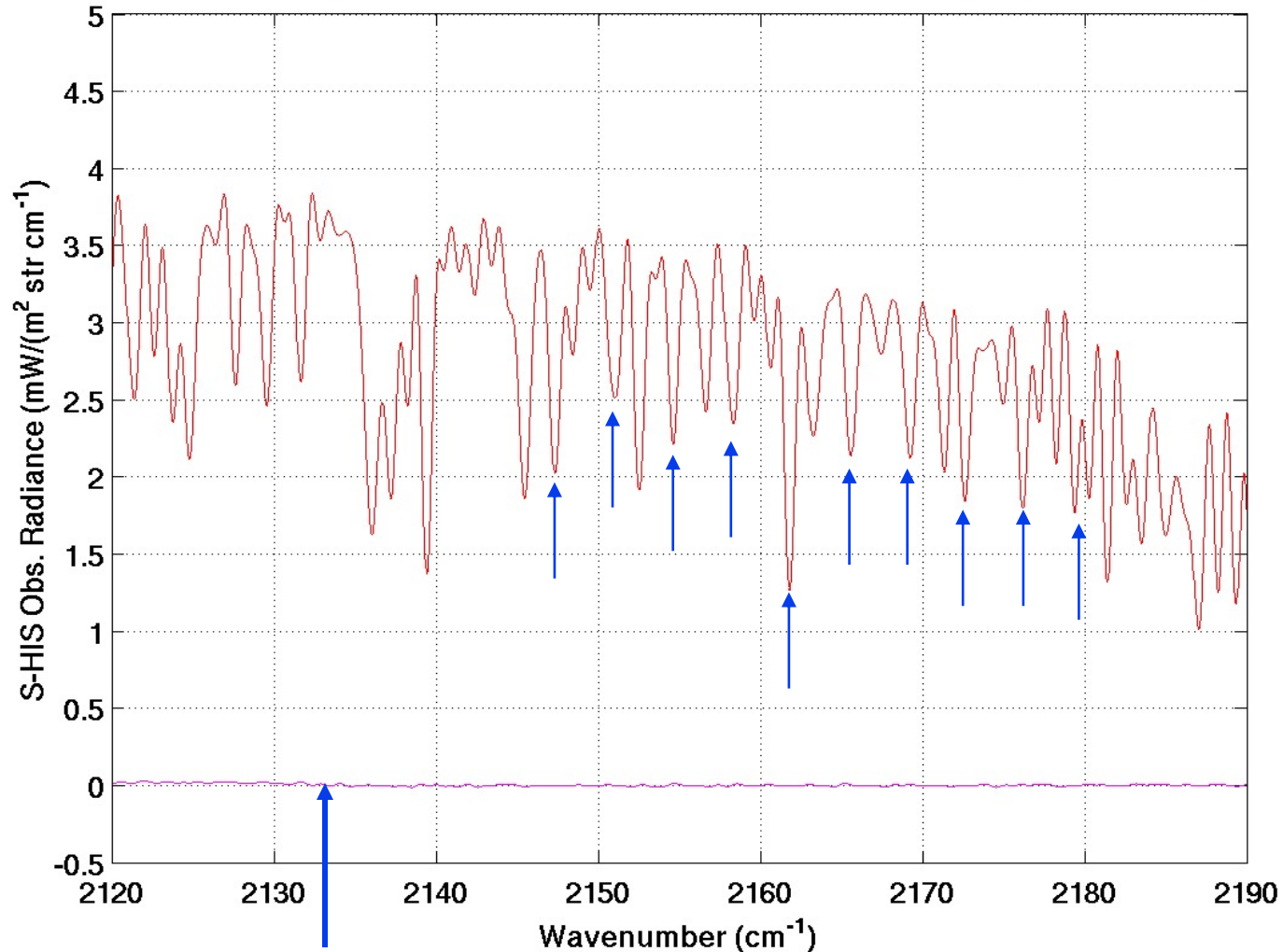
S-HIS zenith and cross-track scanning Earth views 11-16-2002 from Proteus @ ~14km



S-HIS Spectra, 4.67 μm CO

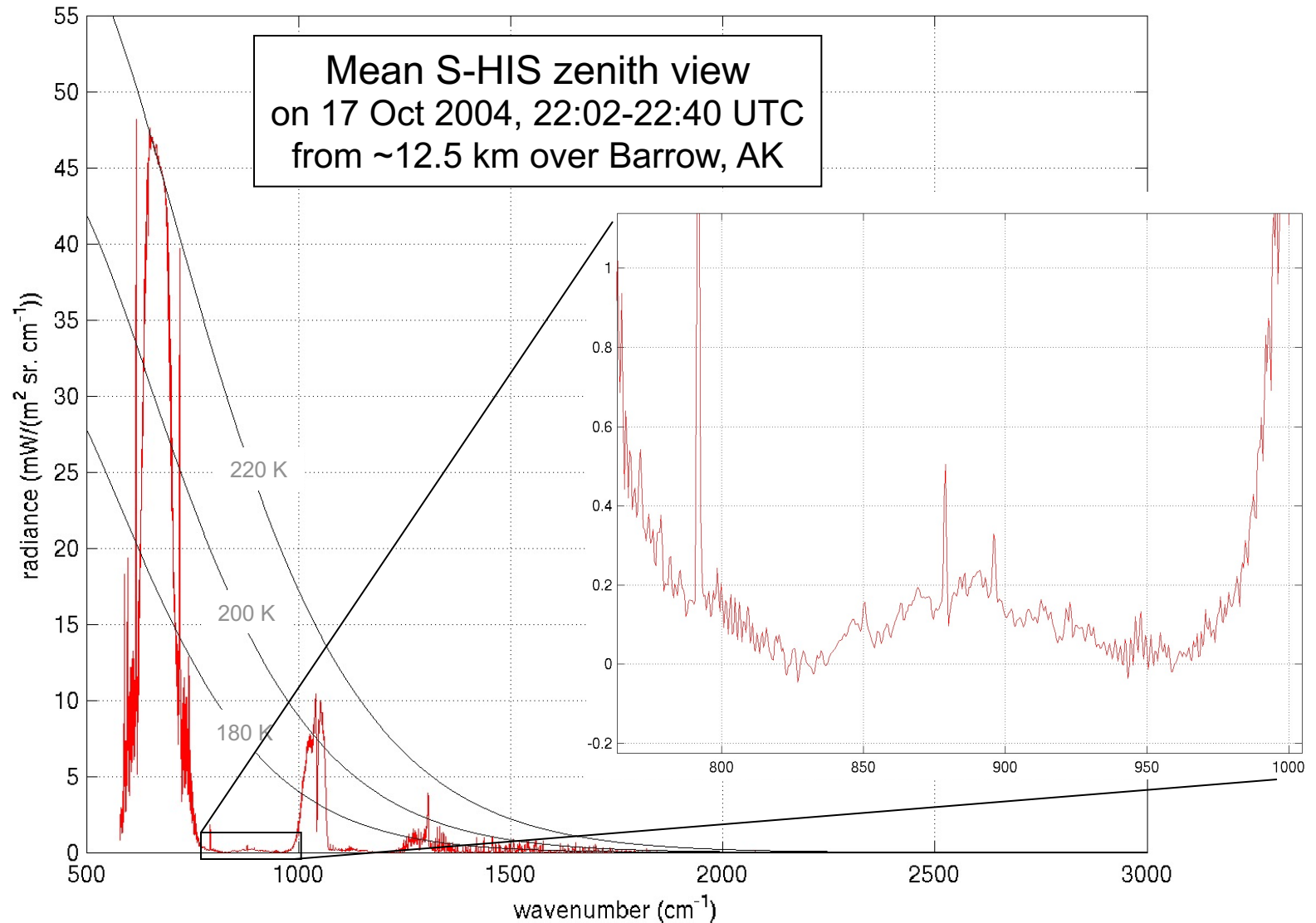
AVE, 26 October 2004

AVE Campaign: 041026 18.4-19.2UTC Zenith/Nadir CO Region(Unapodized)



Note good uplooking zero

HNO₃ in S-HIS Zenith views

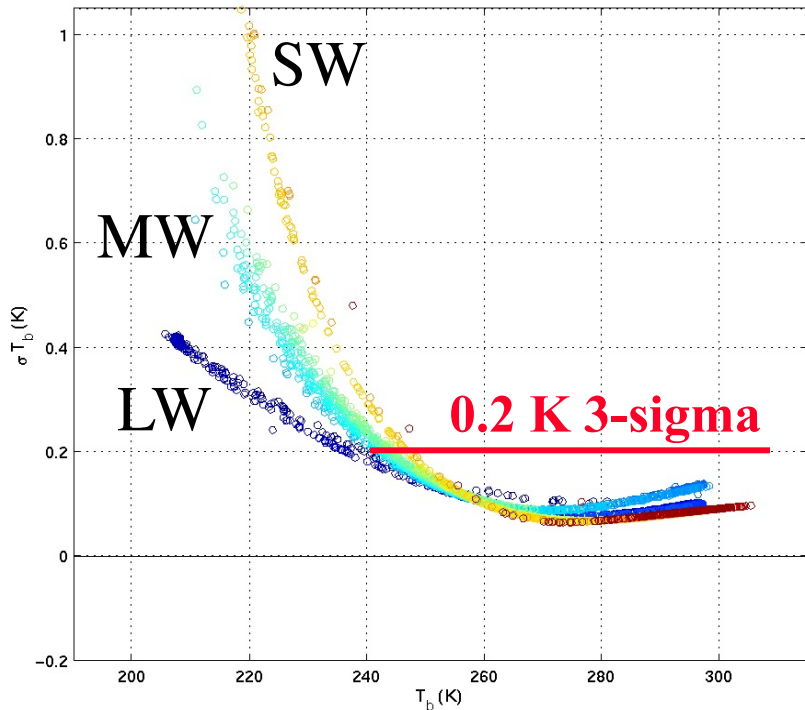




2. S-HIS Radiometric & Spectral Calibration



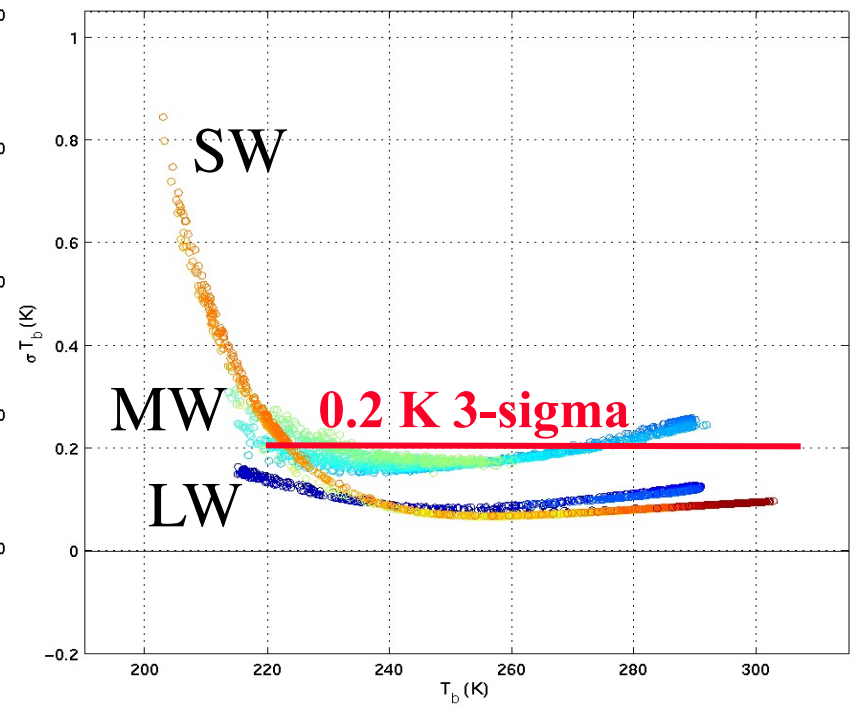
Scanning-HIS Radiometric Calibration 3-sigma Error Budget



← 240K 310K →

Scene Brightness temperature

ER2, 21 Nov 2002
 $T_{ABB} = 260K, T_{HBB} = 310K$



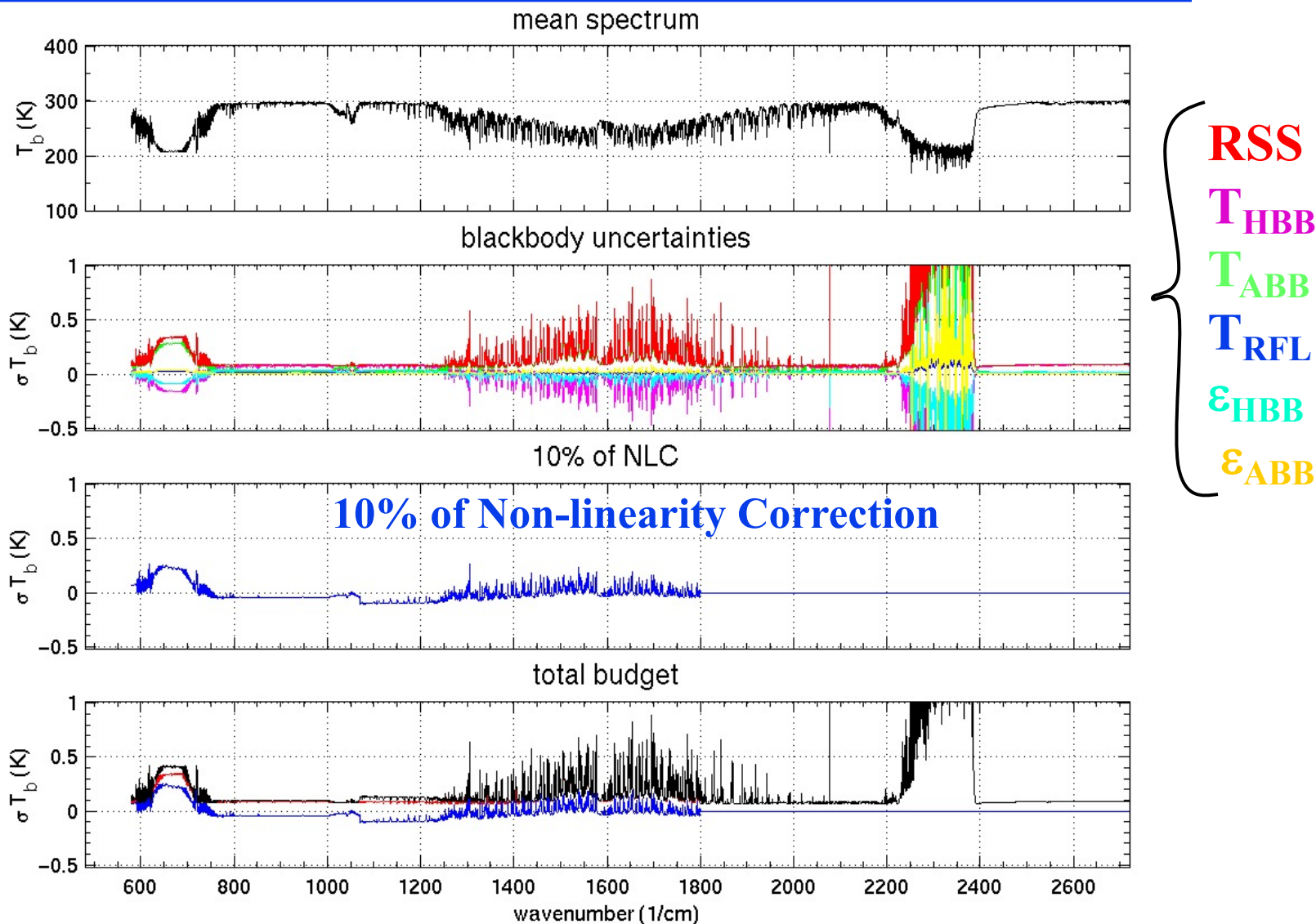
← 220K 310K →

Proteus, 16 Nov 2002
 $T_{ABB} = 227K, T_{HBB} = 310K$

Scanning-HIS Radiometric Calibration Budget

TABB= 260, THBB=310, 11/21/02 ER2

****3-sigma Uncertainties, similar to Best, et al., CALCON 2003 for AERI**



Non-linearity Correction

- ◆ Physical model is basis for correction needing one key coefficient per band
- ◆ Band-to-band overlaps are used to constrain the LW and MW band coefficients
 - SW band detector is highly linear, allowing SW overlap with MW to constrain or test the MW non-linearity
 - MW overlap with LW can then constrain or test the LW non-linearity
- ◆ Up-looking constraints also used to refine non-linearity coefficients and their uncertainties
- ◆ AERI comparisons used for Validation

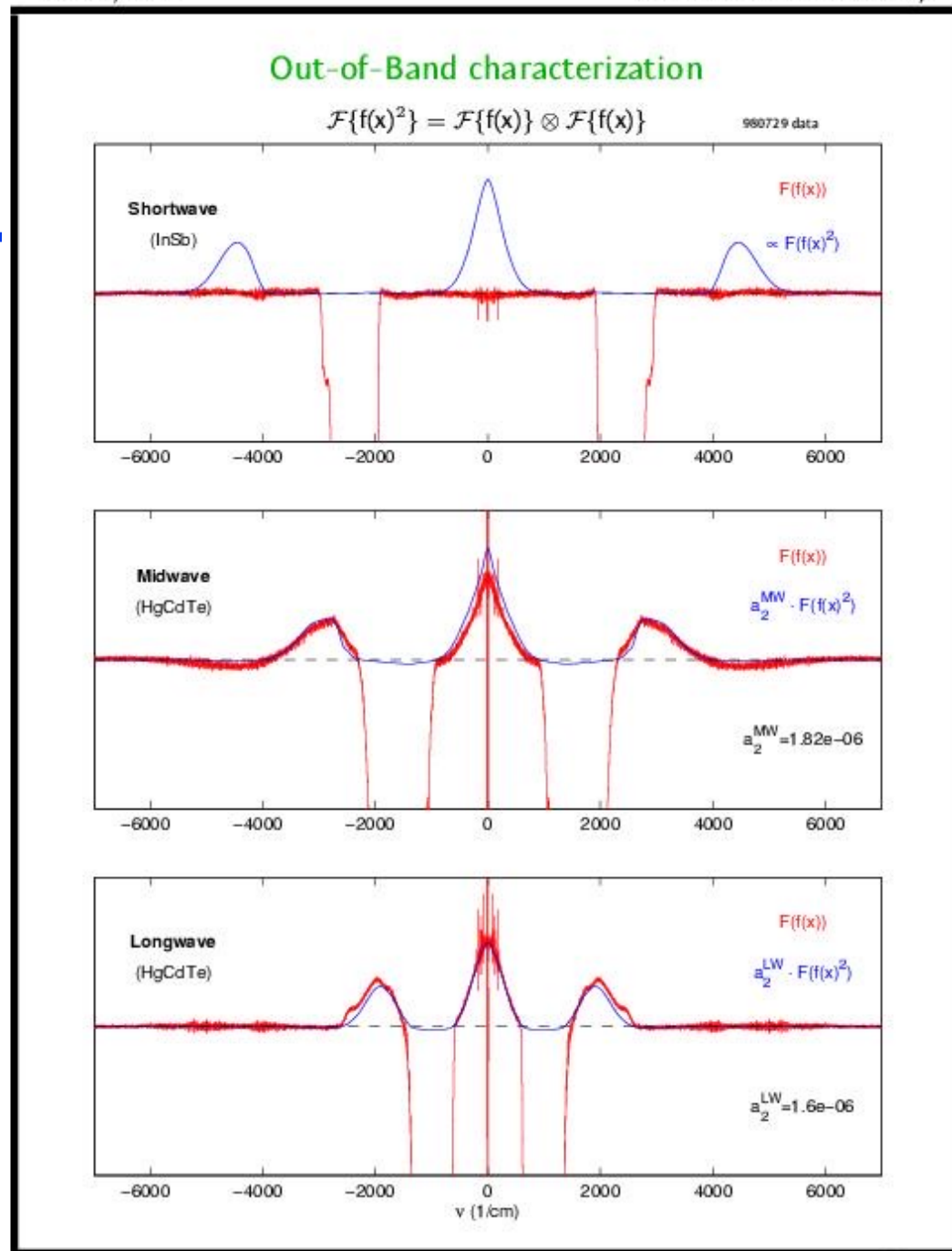
Example Non-linearity: NAST Aircraft Instrument

Out of band response is a good test of linearity & helps define correction

Photo-voltaic InSb detector demonstrates expected high degree of linearity in SW

Photo-conductive HgCdTe demonstrates expected non-linearity in MW & LW

Supports expected quadratic non-linearity of PC detectors



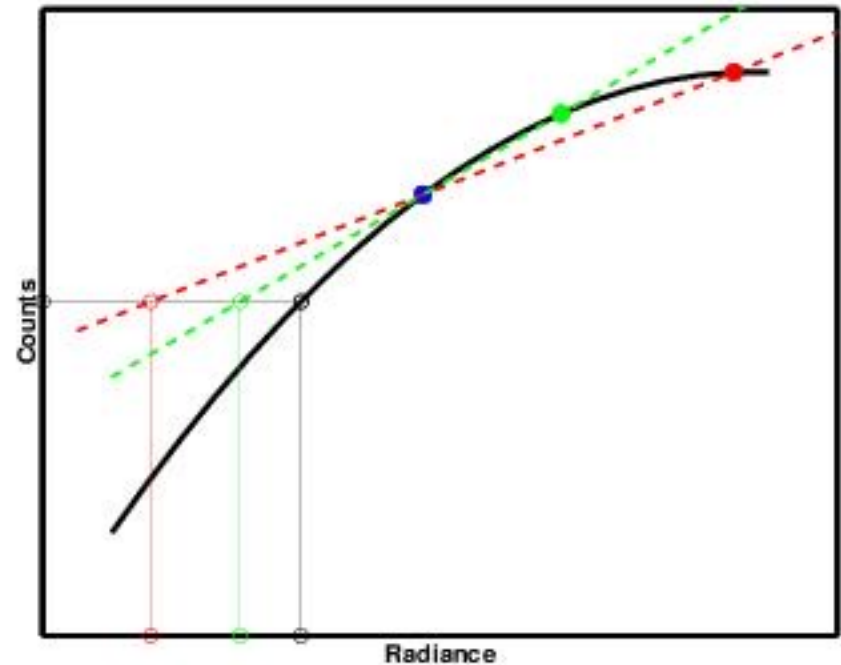
Physical Non-linearity Model, General Principle

- HgCdTe detector theory predicts

$$Q = c_1 \Delta n + c_2 (\Delta n)^2 + c_3 (\Delta n)^3$$
 where Q is the incident photon flux density and Δn is the photo-generated conduction band electron concentration. (Marion B. Reine, 1979)
- The measured signal, I_m , is proportional to Δn , and the corrected linear signal, I_c , is proportional to Q :

$$I_c = I_m + a_2 (I_m)^2 + a_3 (I_m)^3$$
- Separating I_m into an AC interferogram, $f(x)$, and a DC offset, V , gives:

$$I_c = (f + V) + a_2 (f + V)^2 + a_3 (f + V)^3$$



a_2 determined from

- Out of Band: $\tilde{I}_c = 0 \rightarrow |a_n| = \tilde{I}_m / \tilde{I}_m^n$
- uplooking clear sky comparisons with AERI
- in-flight clear sky comparisons with HIS
- comparisons with external blackbodies

Primary Term-Linear in Spectrum

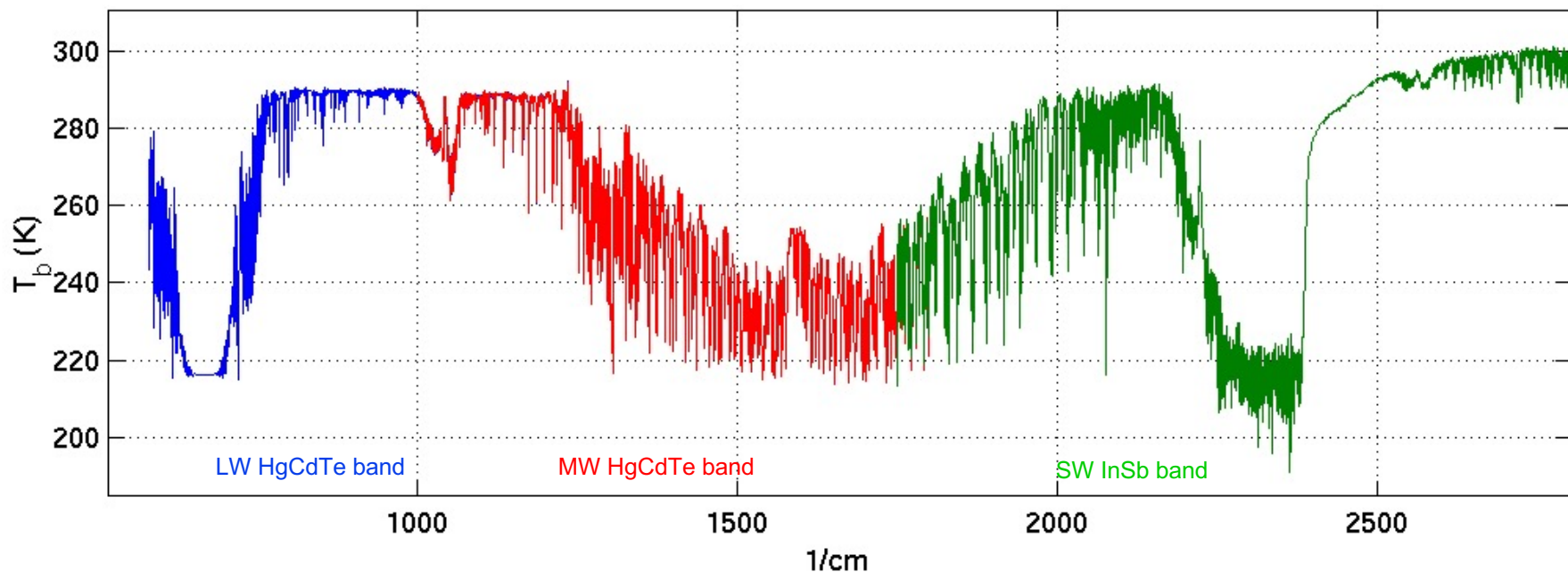
$$\rightarrow \tilde{I}_c = (1 + 2a_2V + 3a_3V^2)\tilde{f} + (a_2 + 3a_3V)\tilde{f}^2 + a_3\tilde{f}^3$$

$$\rightarrow V = \frac{V_a}{e} + \frac{V_a}{e} \frac{k+2r_{dw}}{\frac{B_a}{B_i}(t_{fw}+r_{fw}-r_{dw})}$$

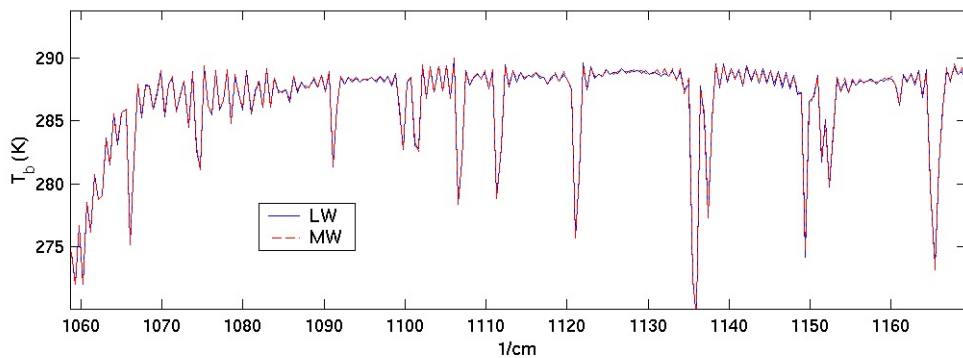
Correction applied before Complex Radiometric Calibration

Scanning-HIS LW/MW and MW/SW Band Overlap

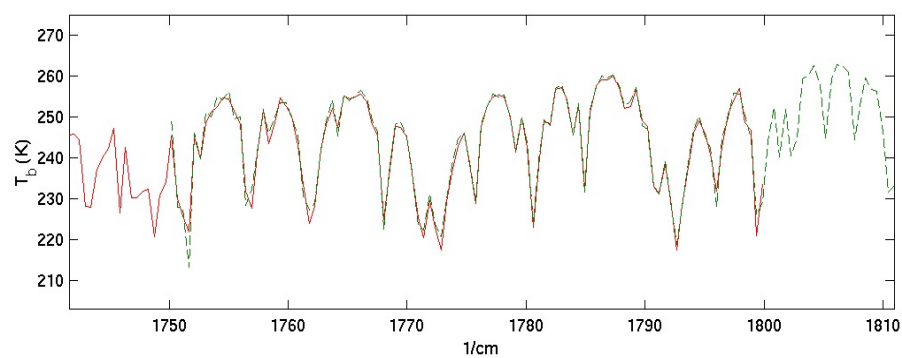
11-16-2002



LW/MW overlap



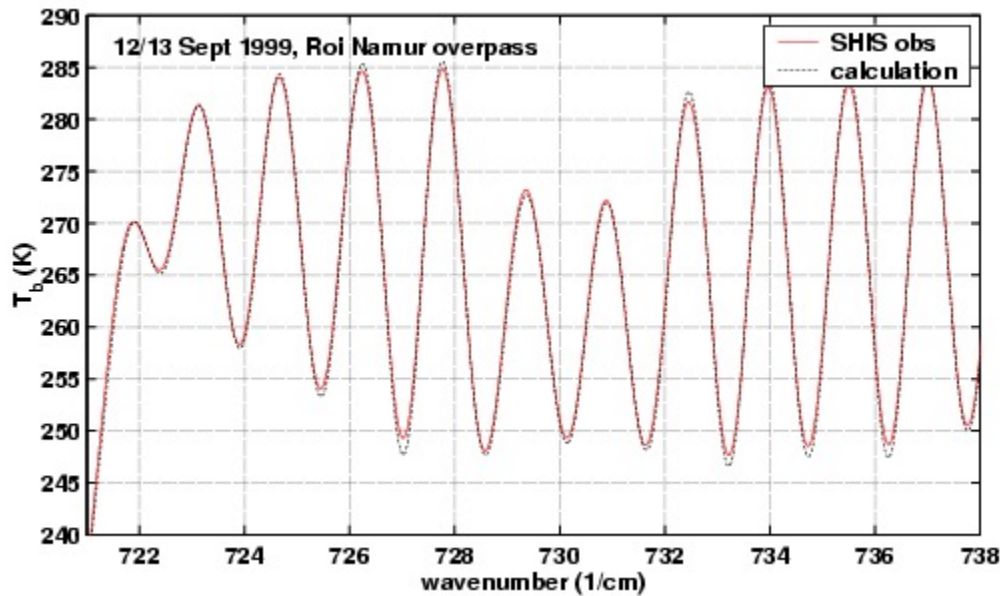
MW/SW overlap



Spectral Calibration and Standardization

- ◆ FTS approach determines the spectral scale for a whole spectral band to within a single multiplicative “scale-stretching” factor
- ◆ The factor is a function of the reference laser wavelength, and the alignment of the laser & IR beams to the interferometer axis, all of which are very stable, even without thermal control
- ◆ **Spectral calibration uses well-known regions of calculated atmospheric spectra off-line & infrequently**
- ◆ **Instrument Line Shape is normalized to an ideal sinc function based on known geometry and refinement using atmospheric nitrous oxide lines near 2195 cm^{-1}**
- ◆ Calibration is followed by procedures to standardize the spectral characteristics

Example Spectral Calibration: S-HIS

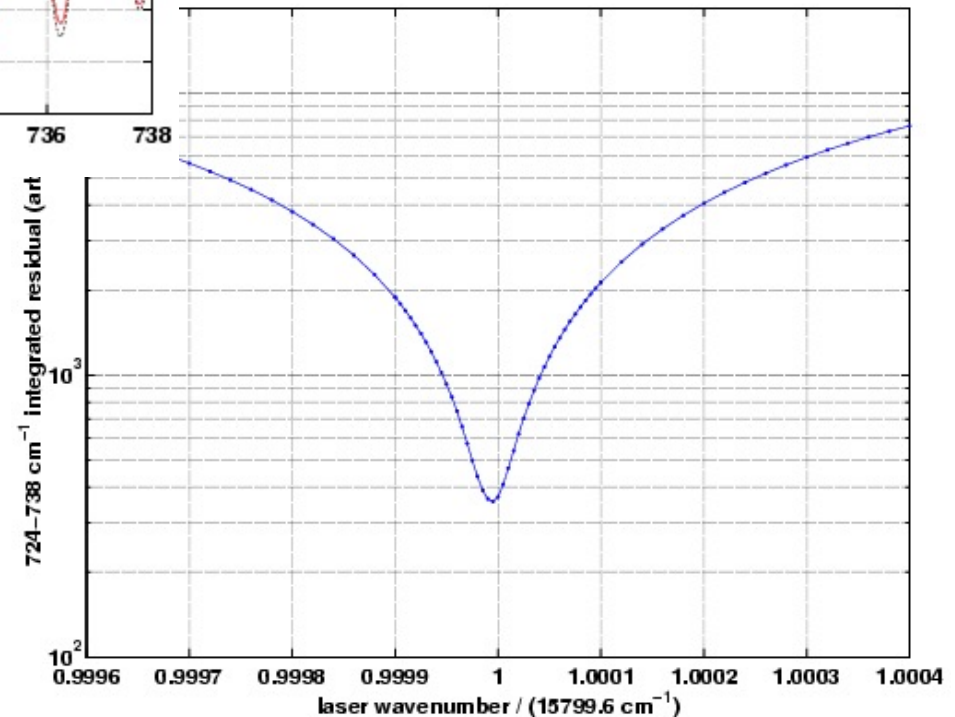


Atmospheric CO₂ lines

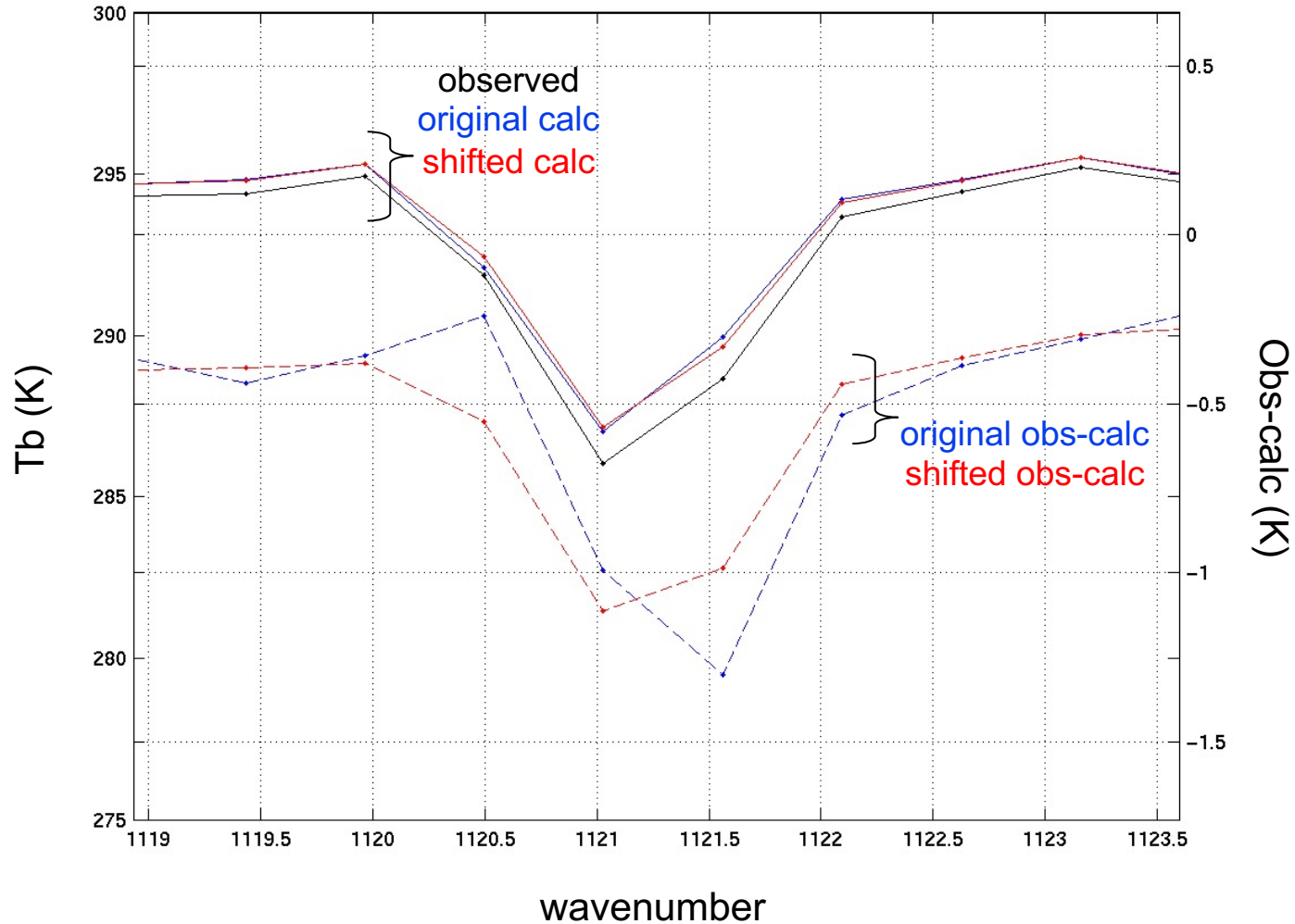
Wavenumber Scale chosen
to minimize difference

Estimated accuracy = 1.2 ppm
(1 sigma)

With many samples,
the accuracy is even higher



Small Spectral Shift (3% of resolution) in AIRS Module-05 identified from S-HIS Validation

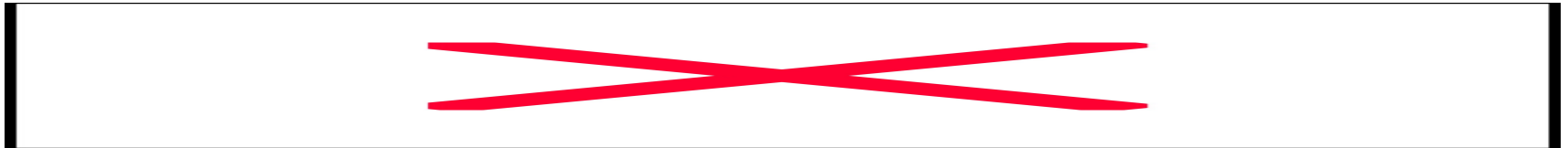


Tobin, et al., CALCON 2003, presented S-HIS Spectral Calibration

Self-Apodization is removed to standardize the Instrument Line Shape (ILS)

Self-apodization function is expanded in a Taylor Series to separate OPD and ν dependence, allowing rigorous relationships in terms of Fourier transforms

- ◆ In expression for the measured interferogram, $F(x)$, expand sinc function as a power series of $(\pi\nu x b^2/2)$:



- ◆ Compute perturbation terms and subtract from measured interferogram.

This process is used for AERI, HIS, S-HIS, NAST-I

Spectral Scale Standardization

- ◆ Producing instrument-independent spectra requires interpolation from the specific instrument scale (determined by spectral calibration) to a standardized scale
- ◆ AERI, HIS, S-HIS and NAST processing implements this interpolation following the self-apodization correction.

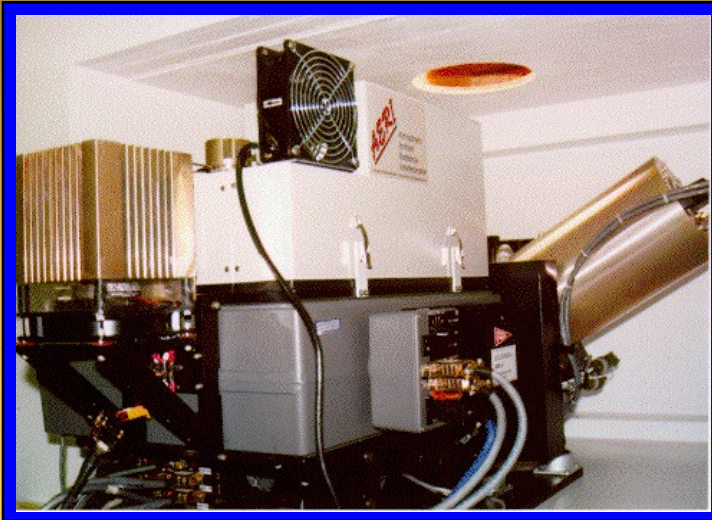
[A densely sampled spectrum, from which linear interpolation can be performed accurately, is constructed by double FFT (FFT calibrated spectrum to interferogram, zero fill to a large effective optical path difference, FFT back to a densely sampled spectrum, and linearly interpolate)]



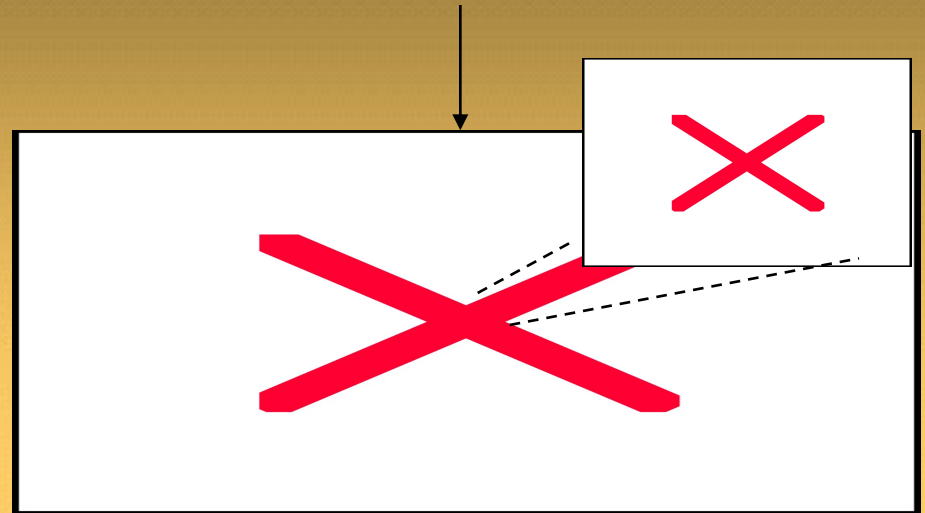
3. Tests of High Spectral Resolution Calibration

ATMOSPHERIC EMITTED RADIANCE INTERFEROMETER (AERI)

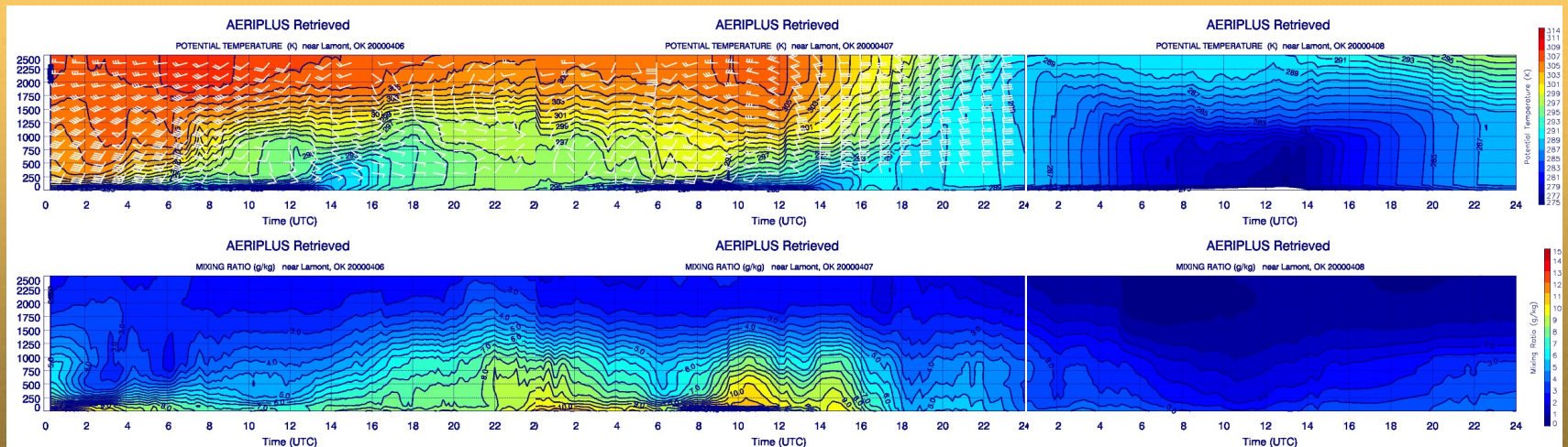
Clear Sky and Cloud Downwelling Emission



Operational at DOE ARM



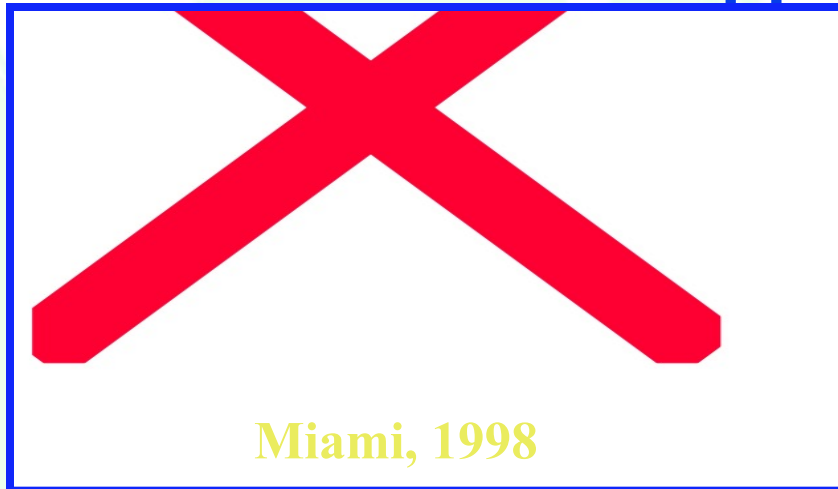
Accurate High Resolution Radiometry



Continuous Atmospheric Profiling - Temperature and Water Vapor

The NIST Connection

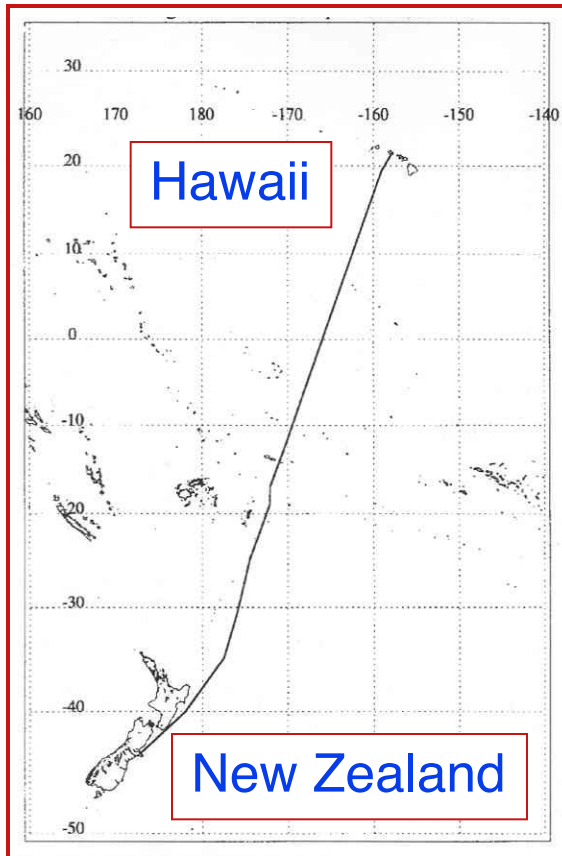
- Comparisons with NIST maintained blackbodies conducted with ground-based AERI. S-HIS employs the same calibration approaches



Max Difference
< 0.055°C Longwave
< 0.035°C Shortwave
between 293 & 333 K

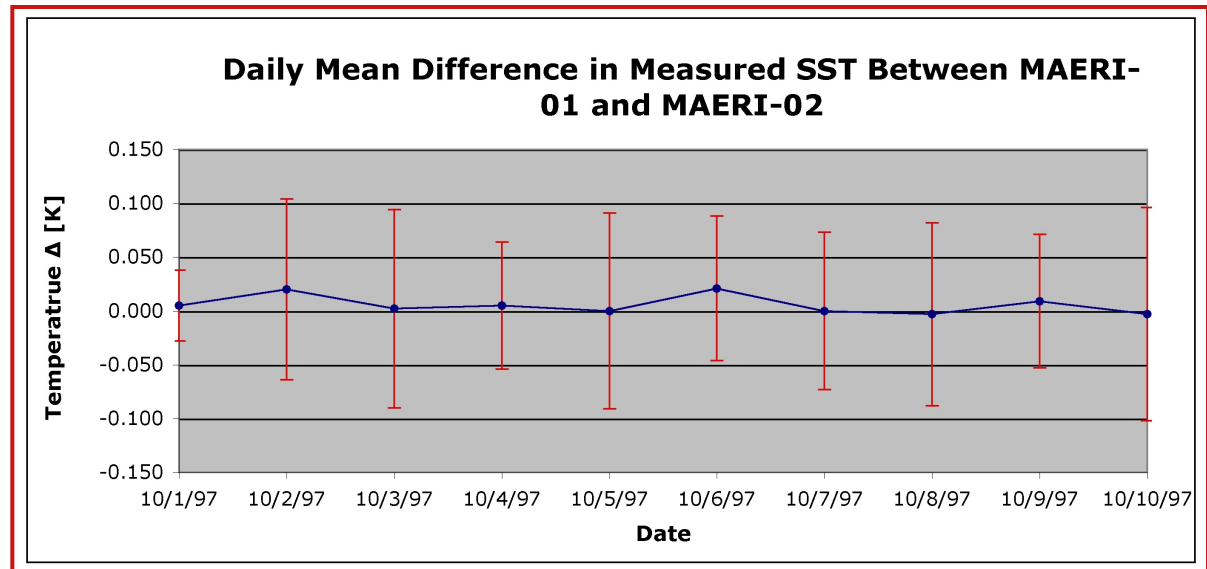
- Direct test of S-HIS planned using NIST Transfer Radiometer (TXR) at aircraft flight temperatures

Intercomparison of 2 Marine AERIs Measuring Sea Surface Temperature



Track of the R/V Roger Revelle
28 Sept. - 14 Oct. 1997

16 Day Cruise

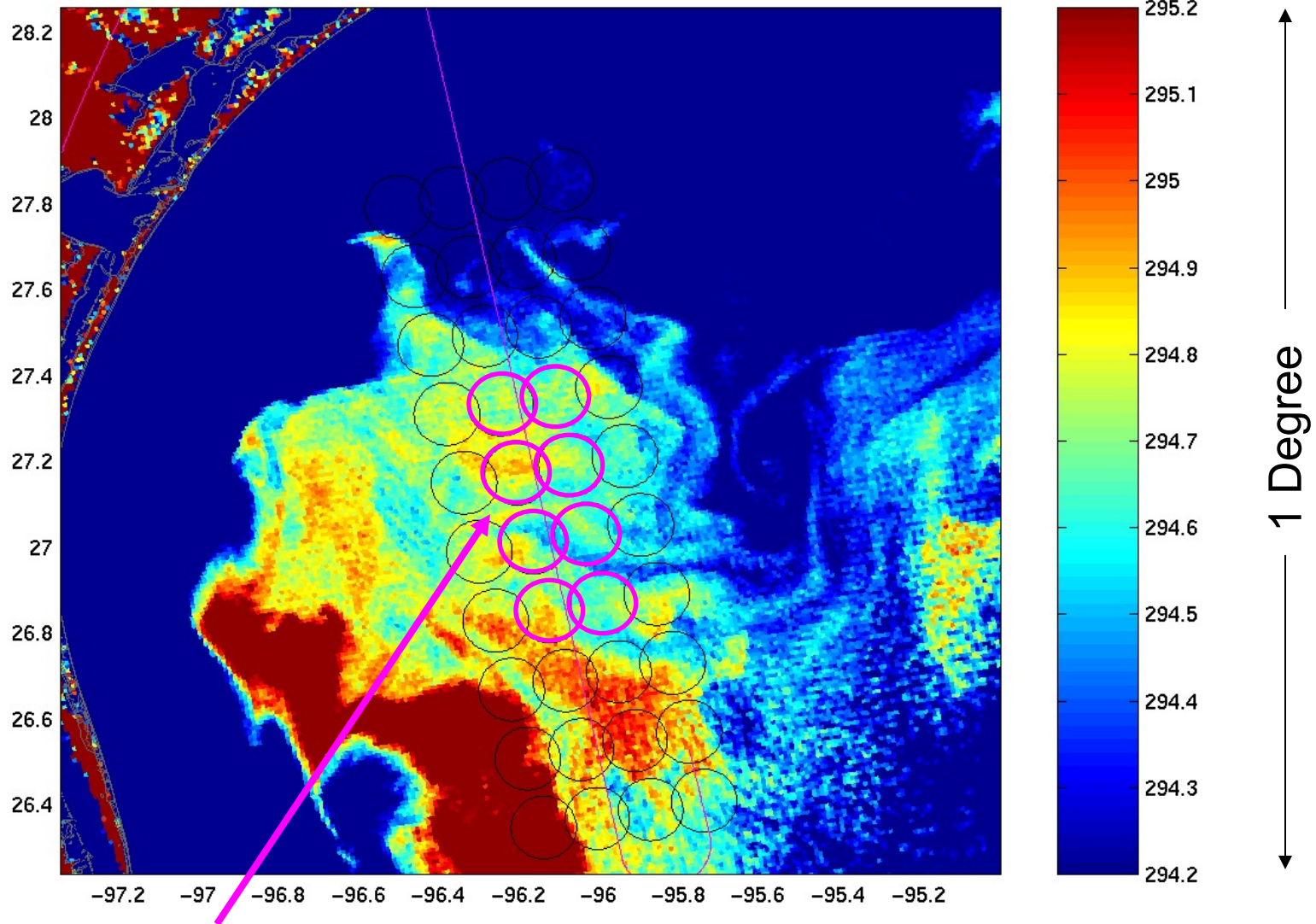


Largest Daily Mean Difference: 0.020 K
Ten Day Mean Difference: 0.005 K



AIRS Validation with UW Scanning HIS

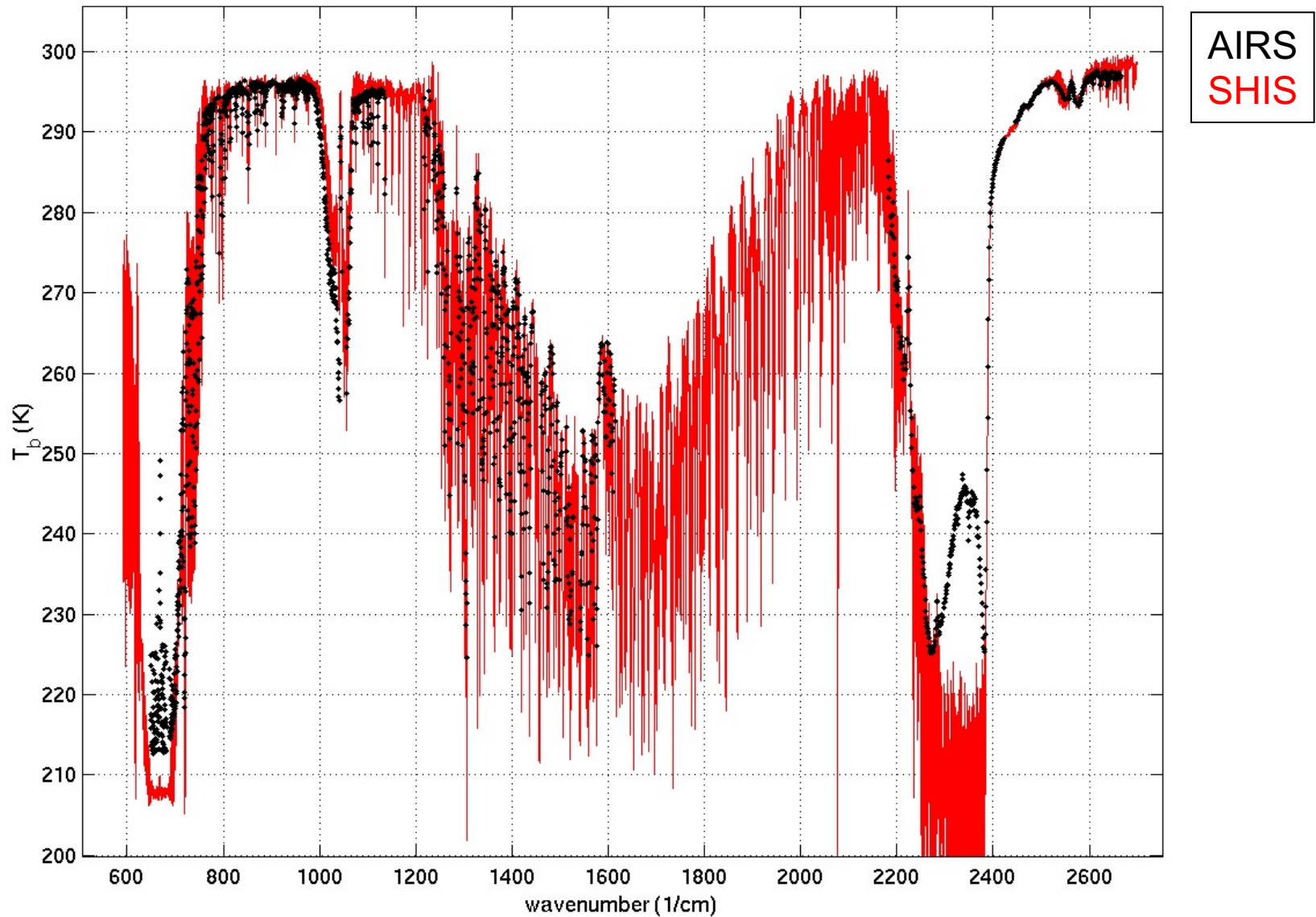
21 November 2002, NASA ER2



**8 AIRS FOVs used in the following comparisons
(shown in MODIS 12 micron image)**

2002 Gulf of Mexico Comparison

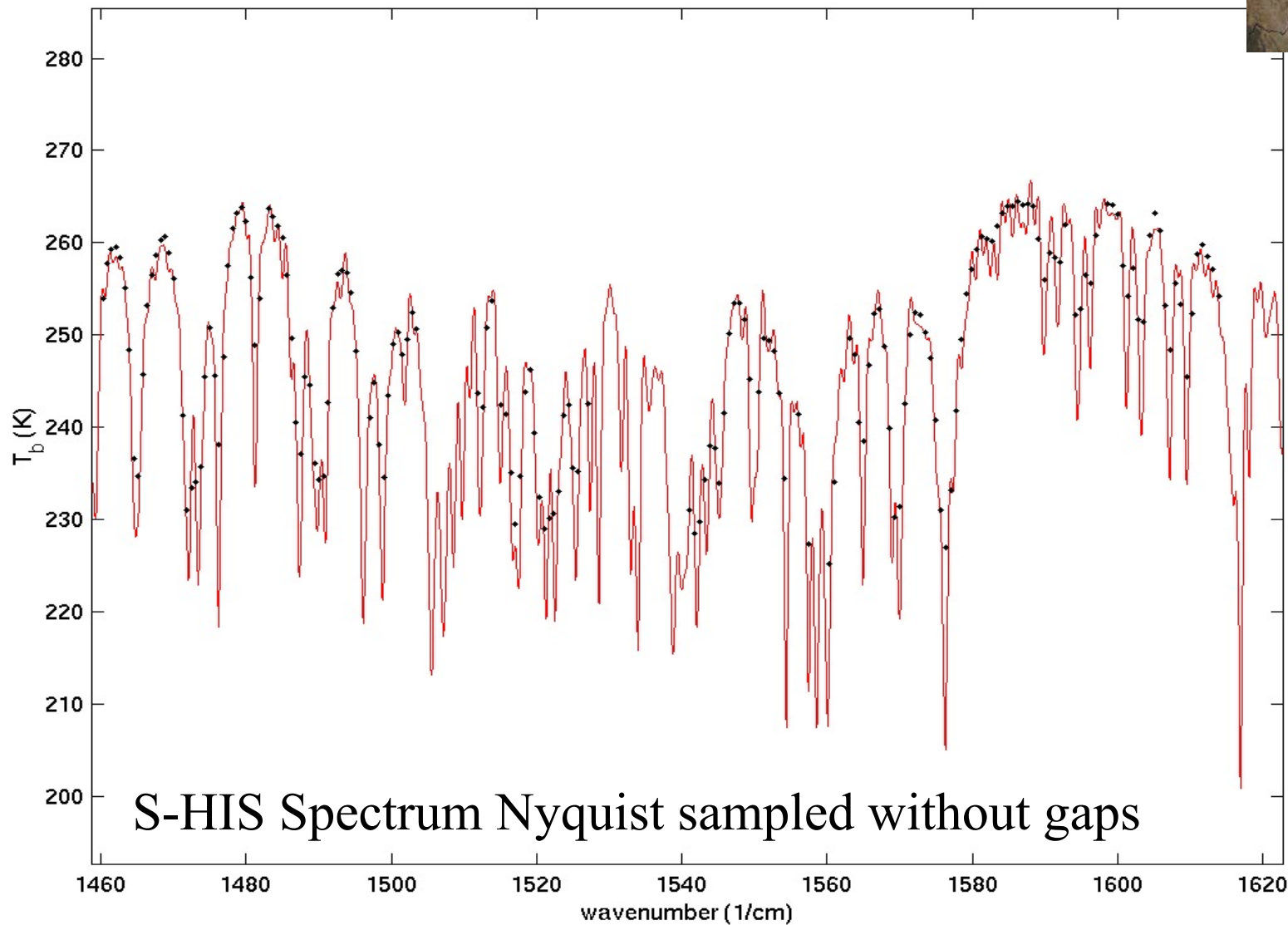
8 AIRS FOVs, 448 SHIS FOVs, PC filtering



“comparison 0”

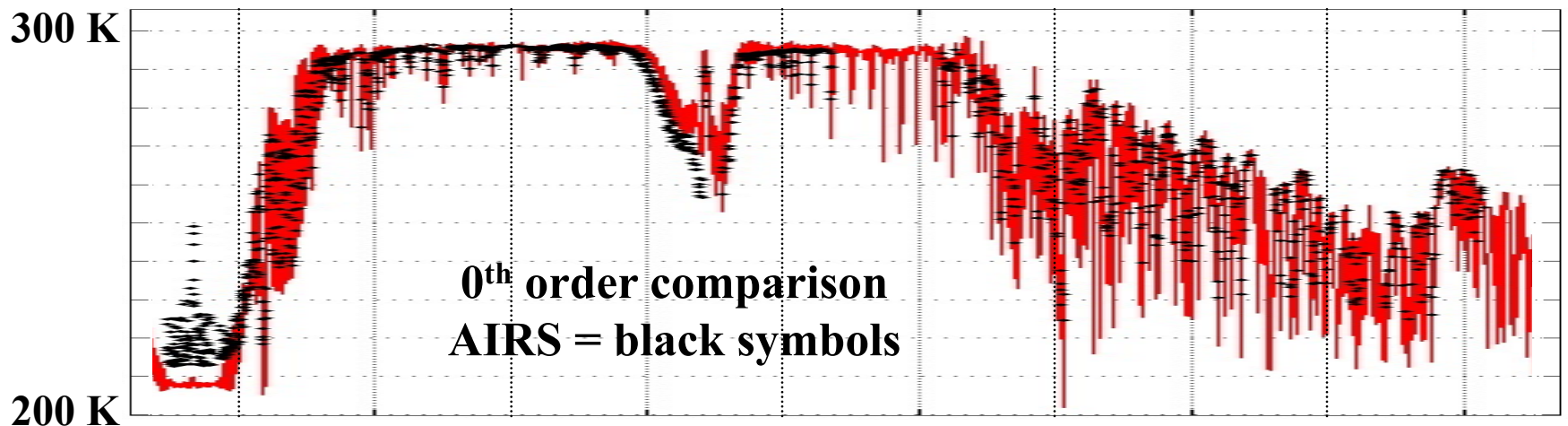
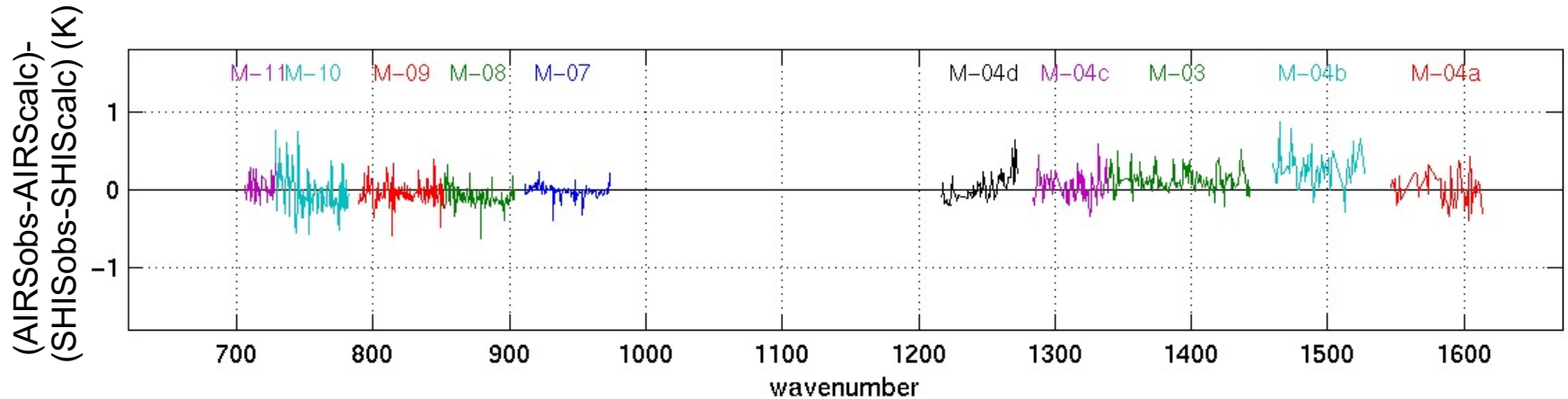
“comparison 0”

8 AIRS FOVs, 448 SHIS FOVs, PC filtering



Detailed Radiance Comparison: Spectrally normalized AIRS-HIS Residuals

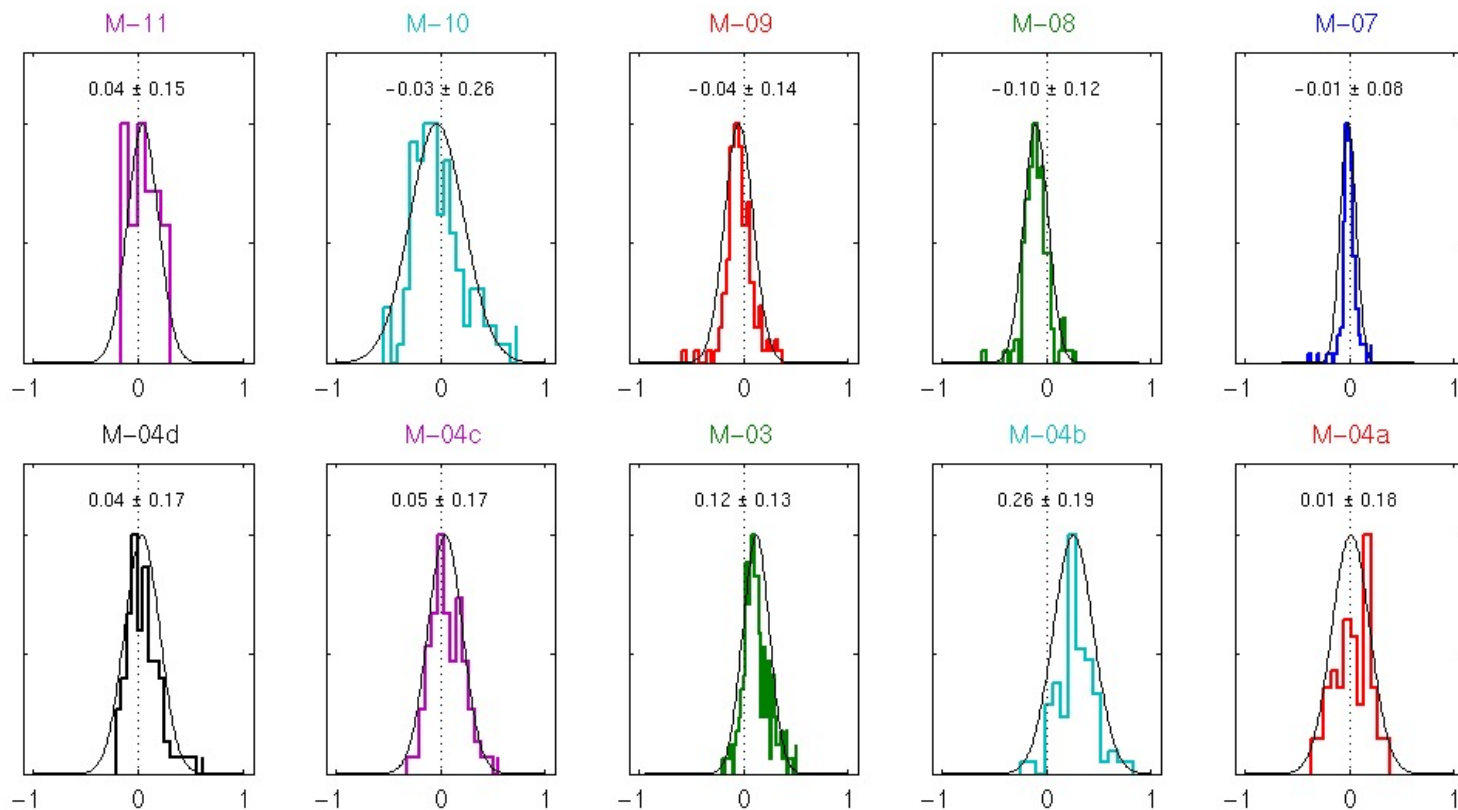
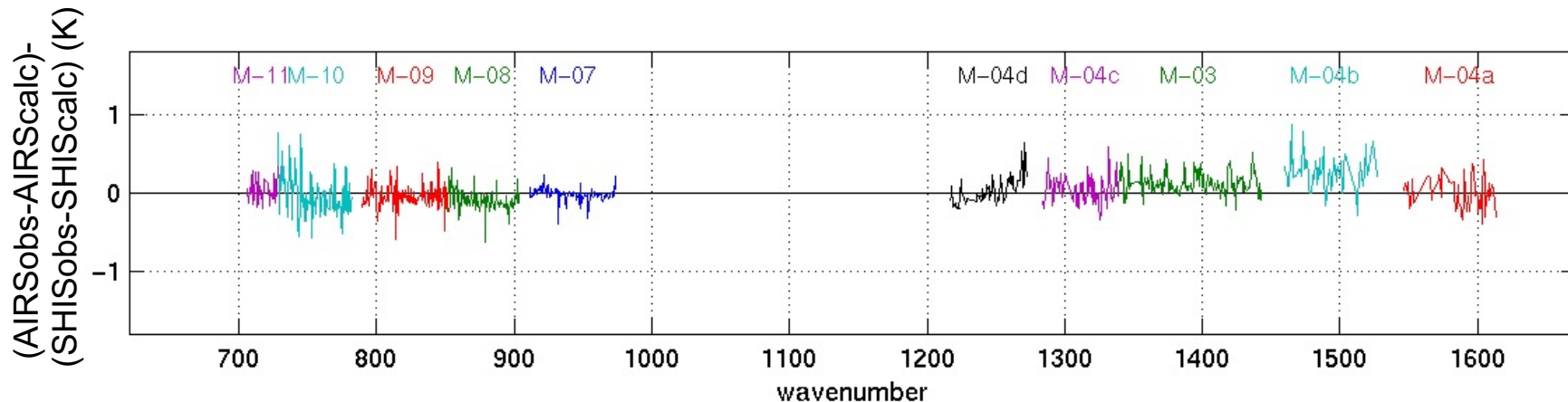
Mean over AIRS modules (same color) generally <0.1 K!



Excluding channels strongly affected by atmosphere above ER2

Statistical Properties of AIRS-SHIS Residuals

Mean generally < 0.1 K & Standard Deviation < 0.2 K over AIRS modules



New Comparisons from 2004 Field Experiments

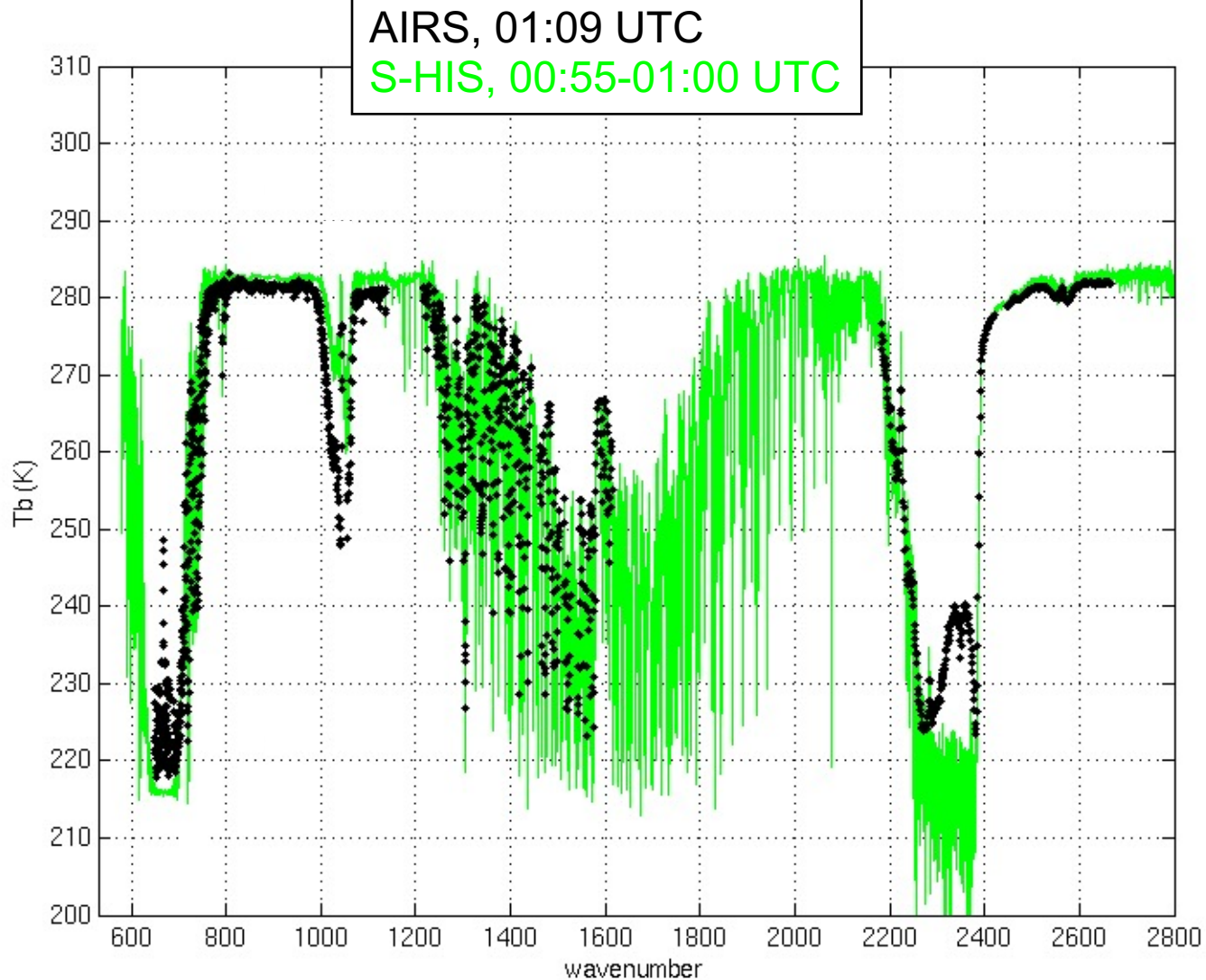
EAQUATE: **E**uropean **A**qua **T**hermal
Experiment (Italy & UK)

MPACE: **M**ixed-**P**hase **A**rctic **C**loud
Experiment

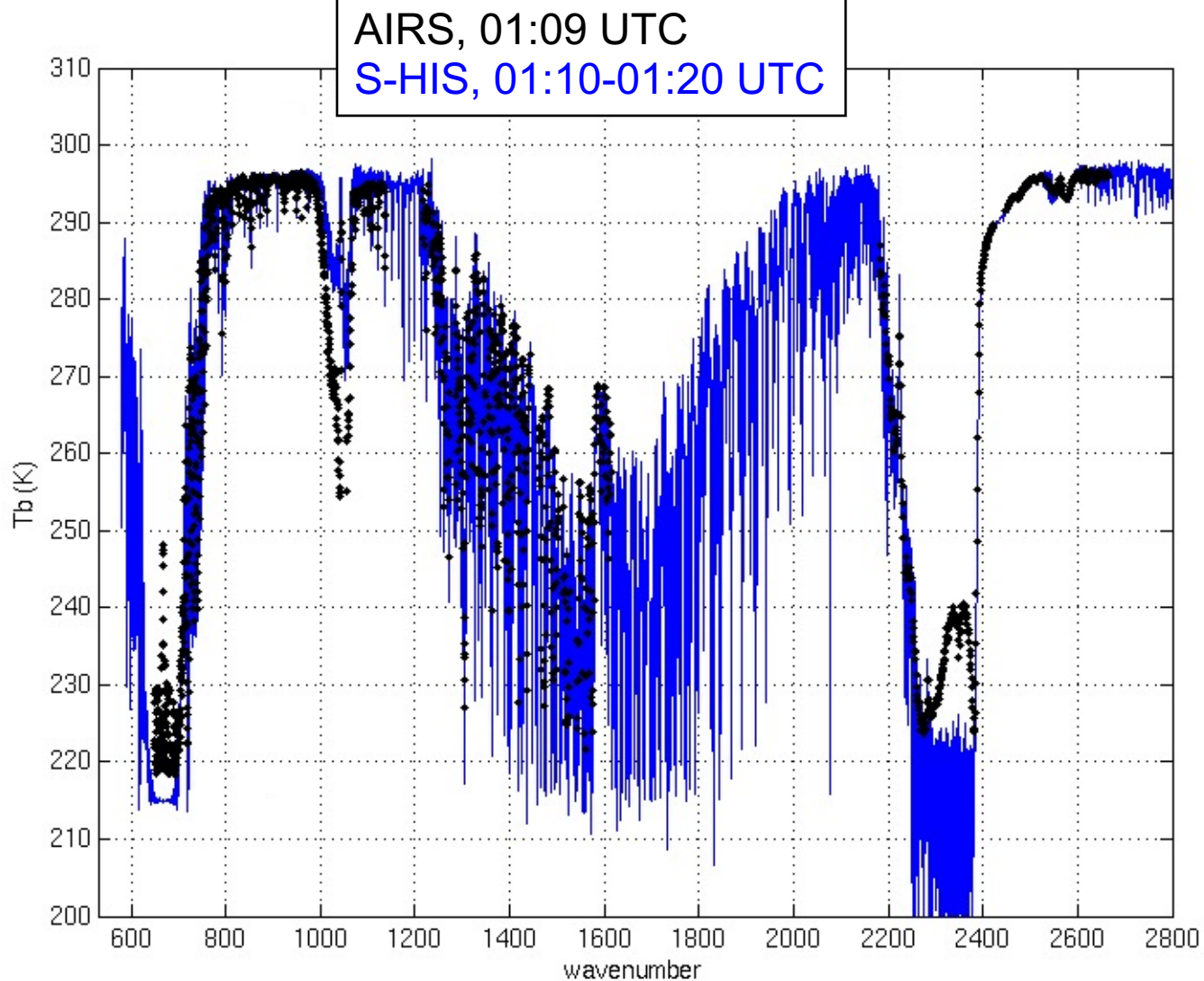
AVE: **A**ura **V**alidation **E**xperiment

Only Processed through 0th order comparison

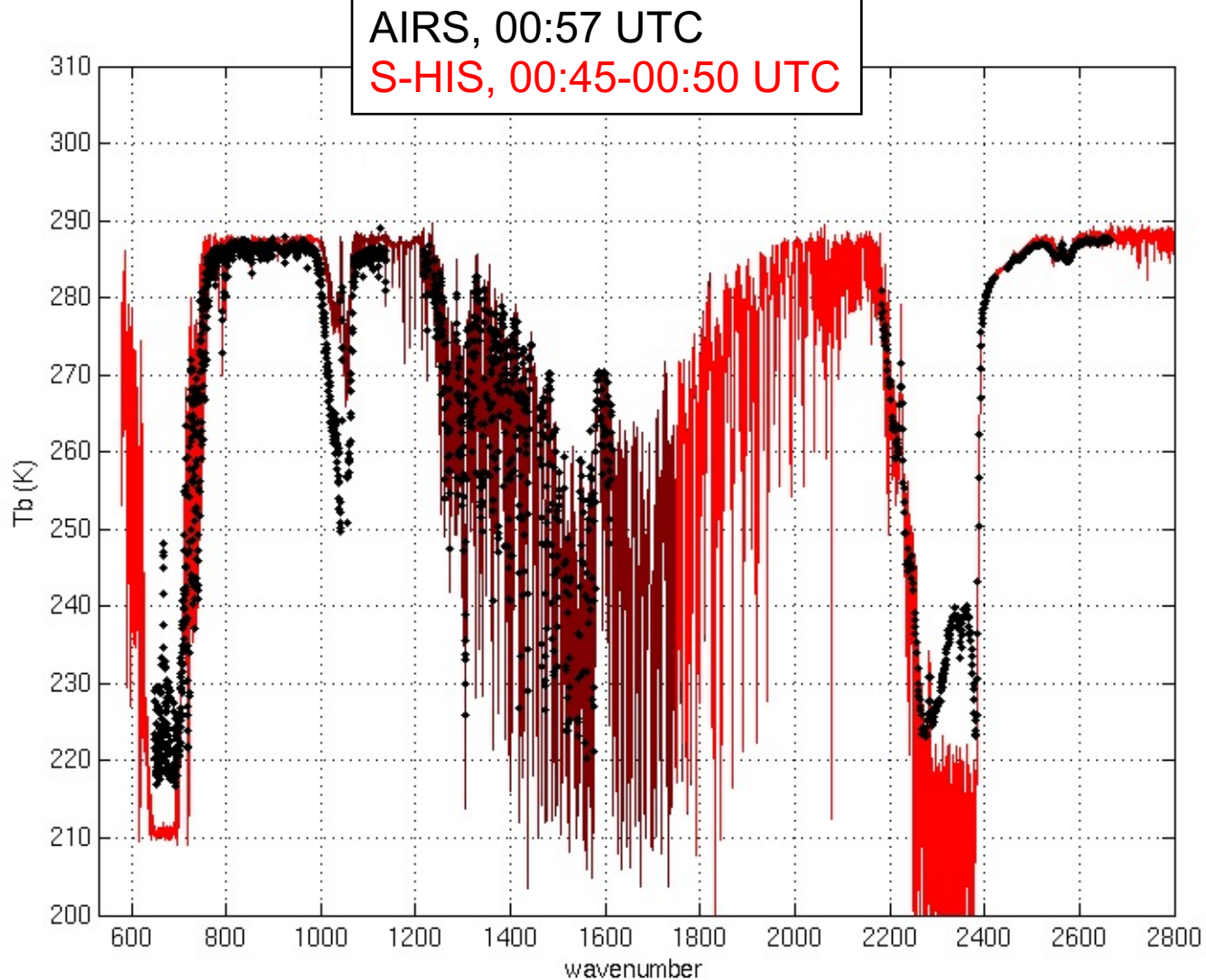
EAQUATE (Italy) 040907- Mountains



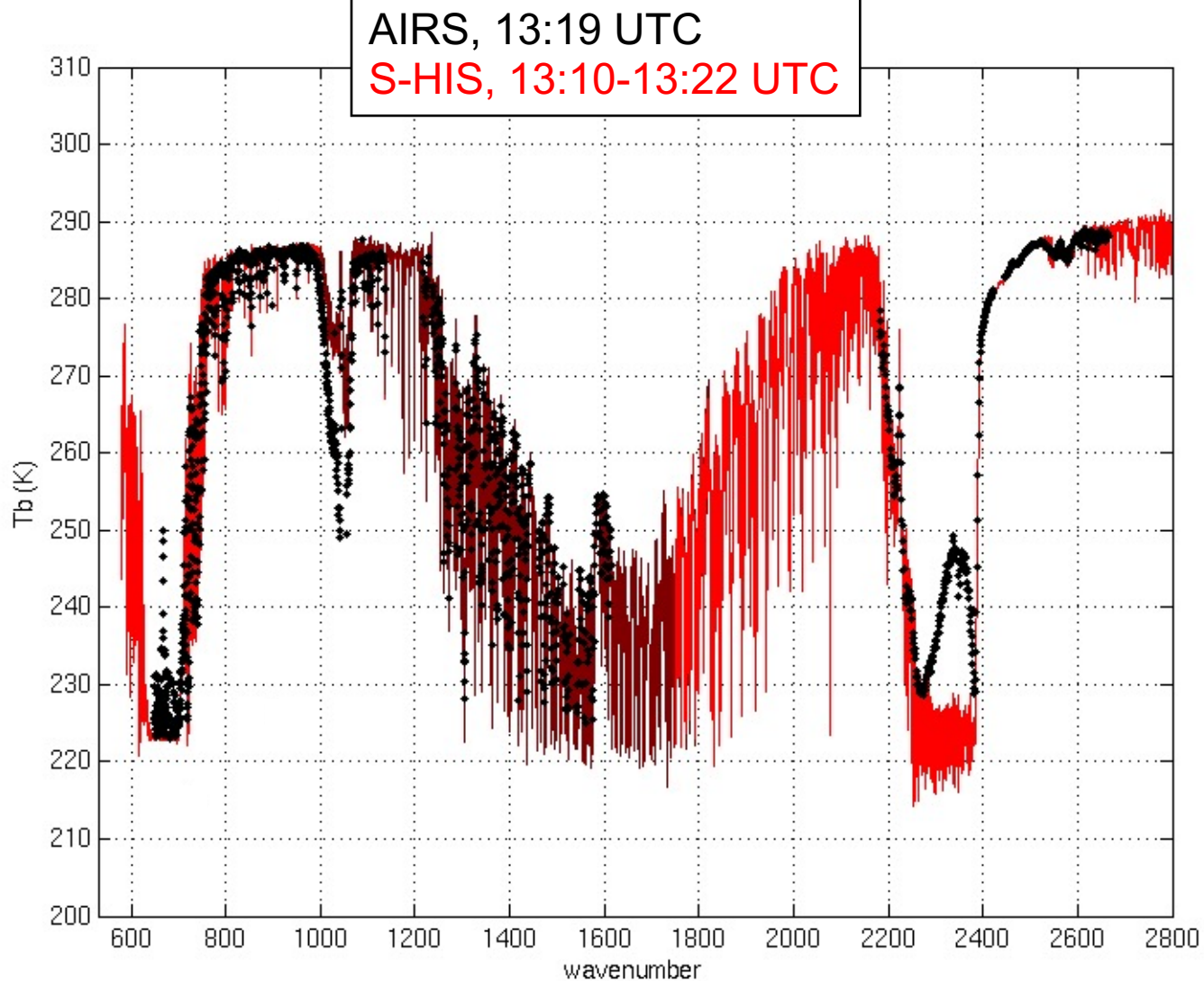
EAQUATE (Italy) 040907- Ocean



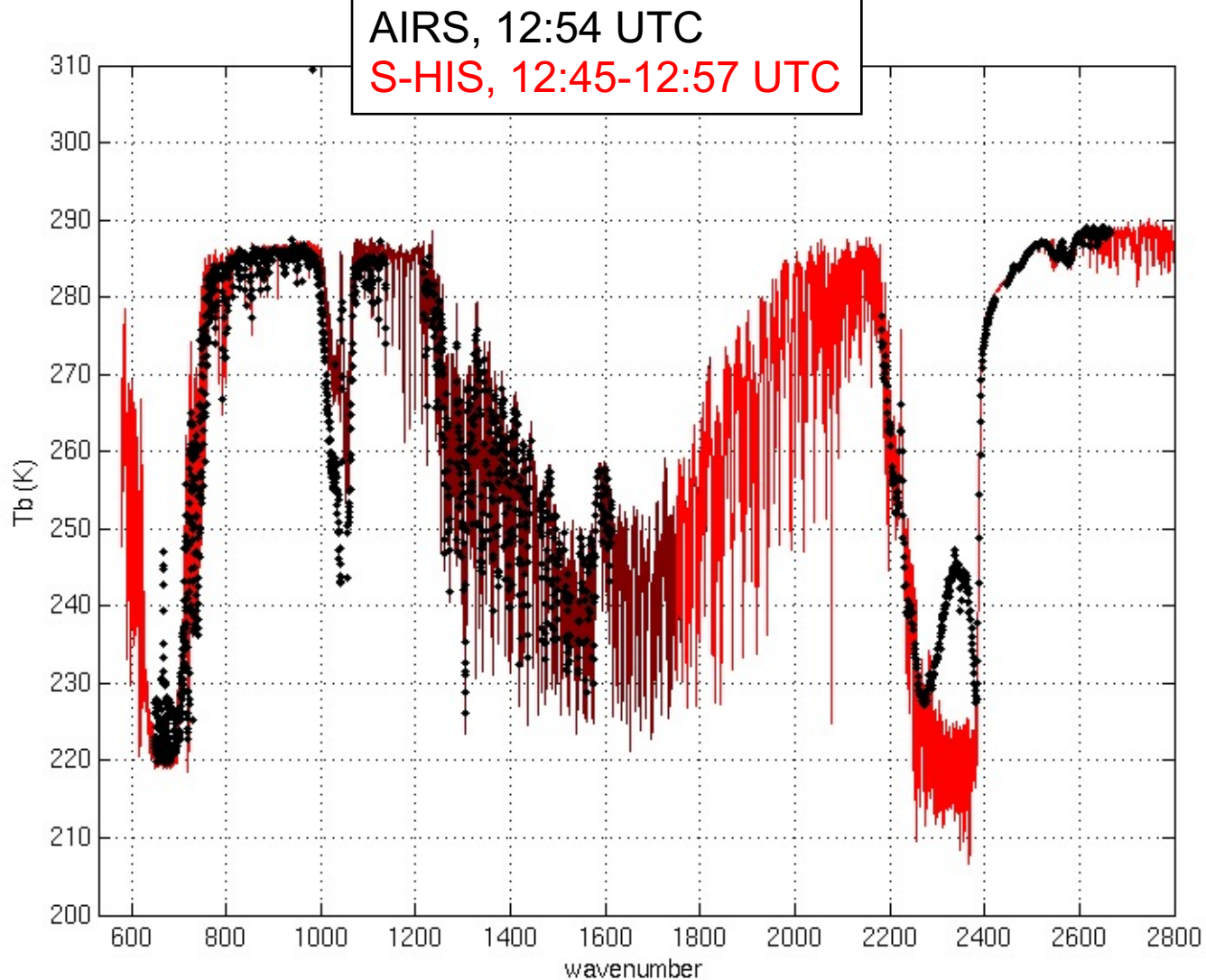
EAQUATE (Italy) 040909



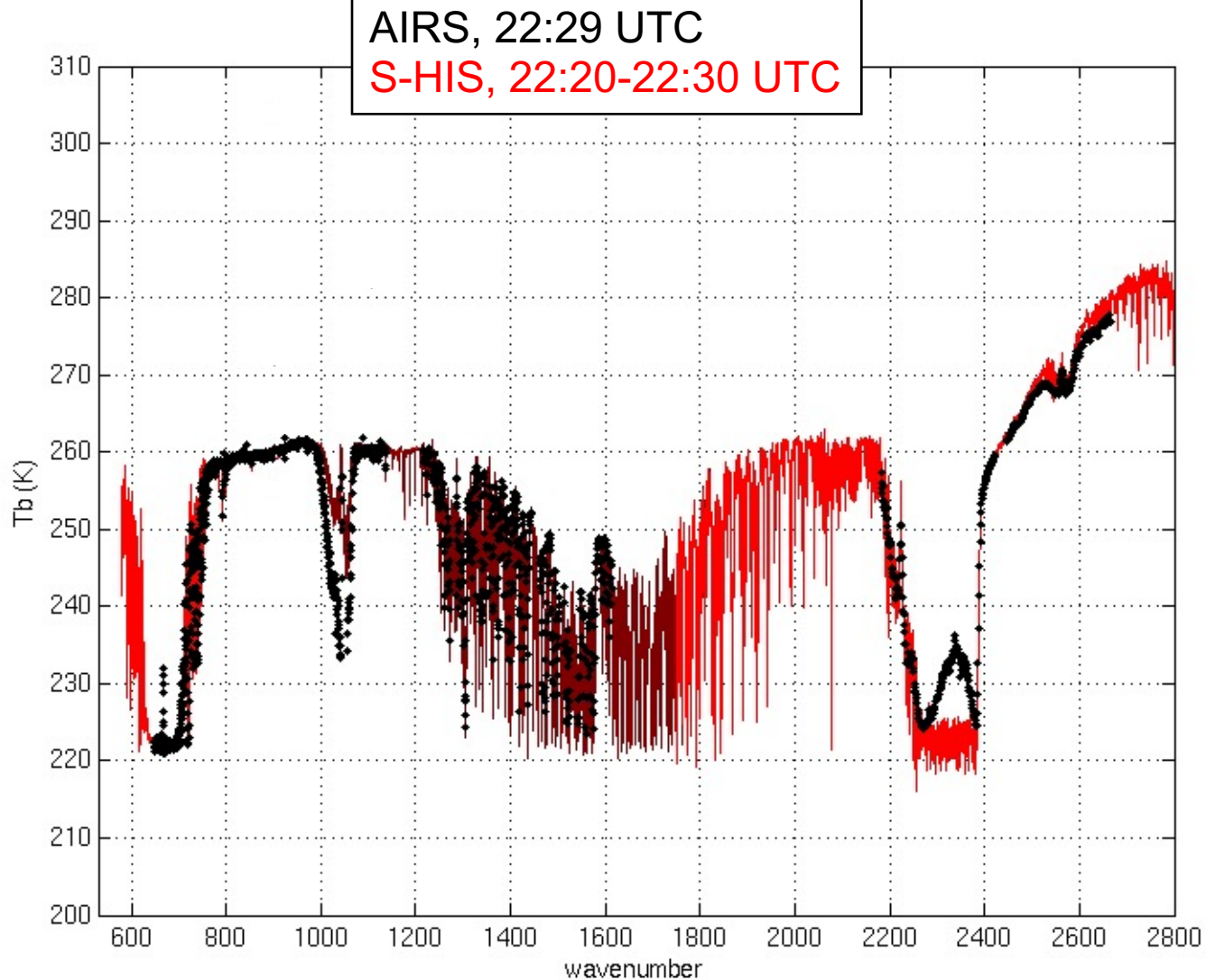
EAQUATE (UK) 040914



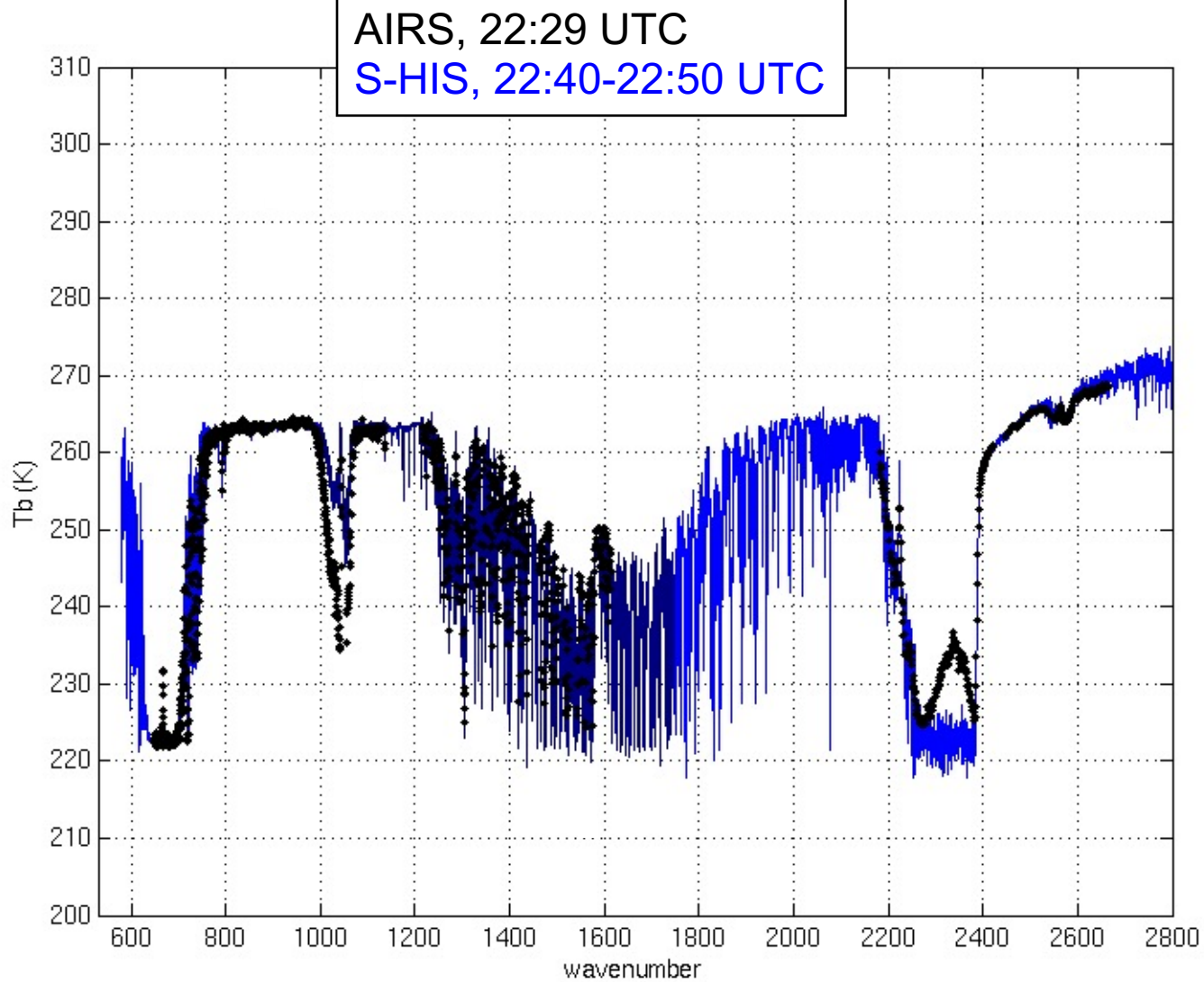
EAQUATE (UK) 040918



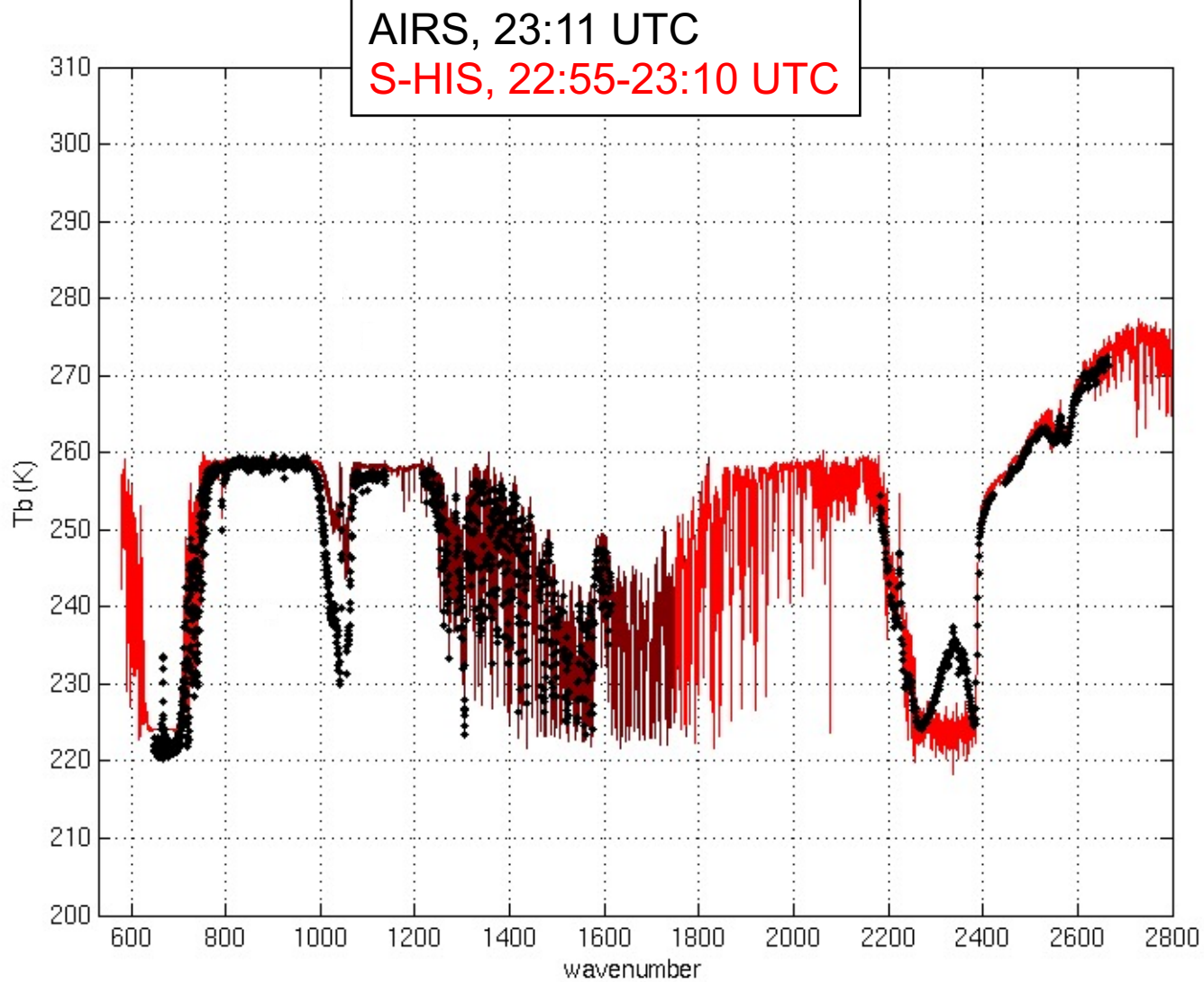
MPACE 10/08



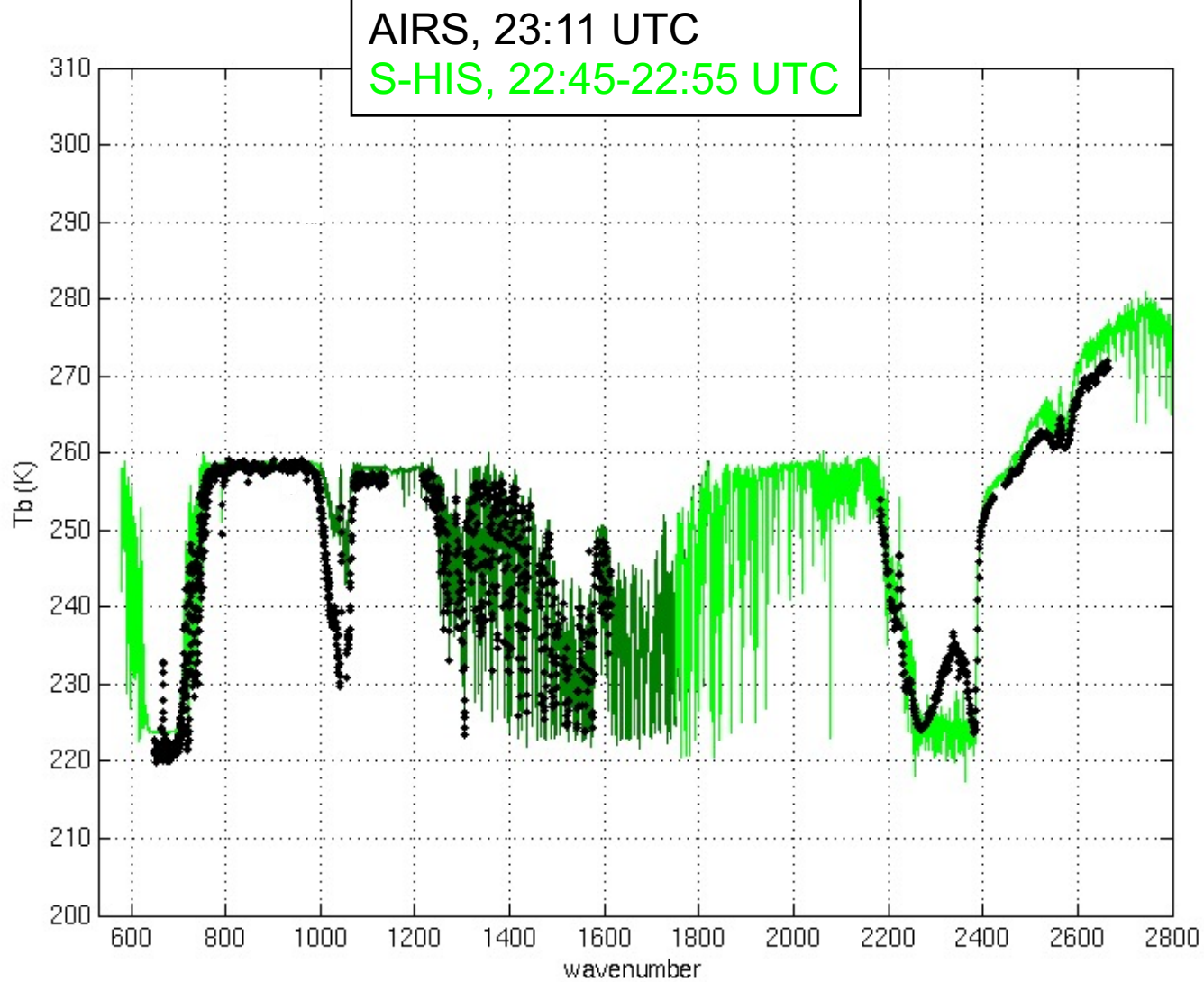
MPACE 10/08



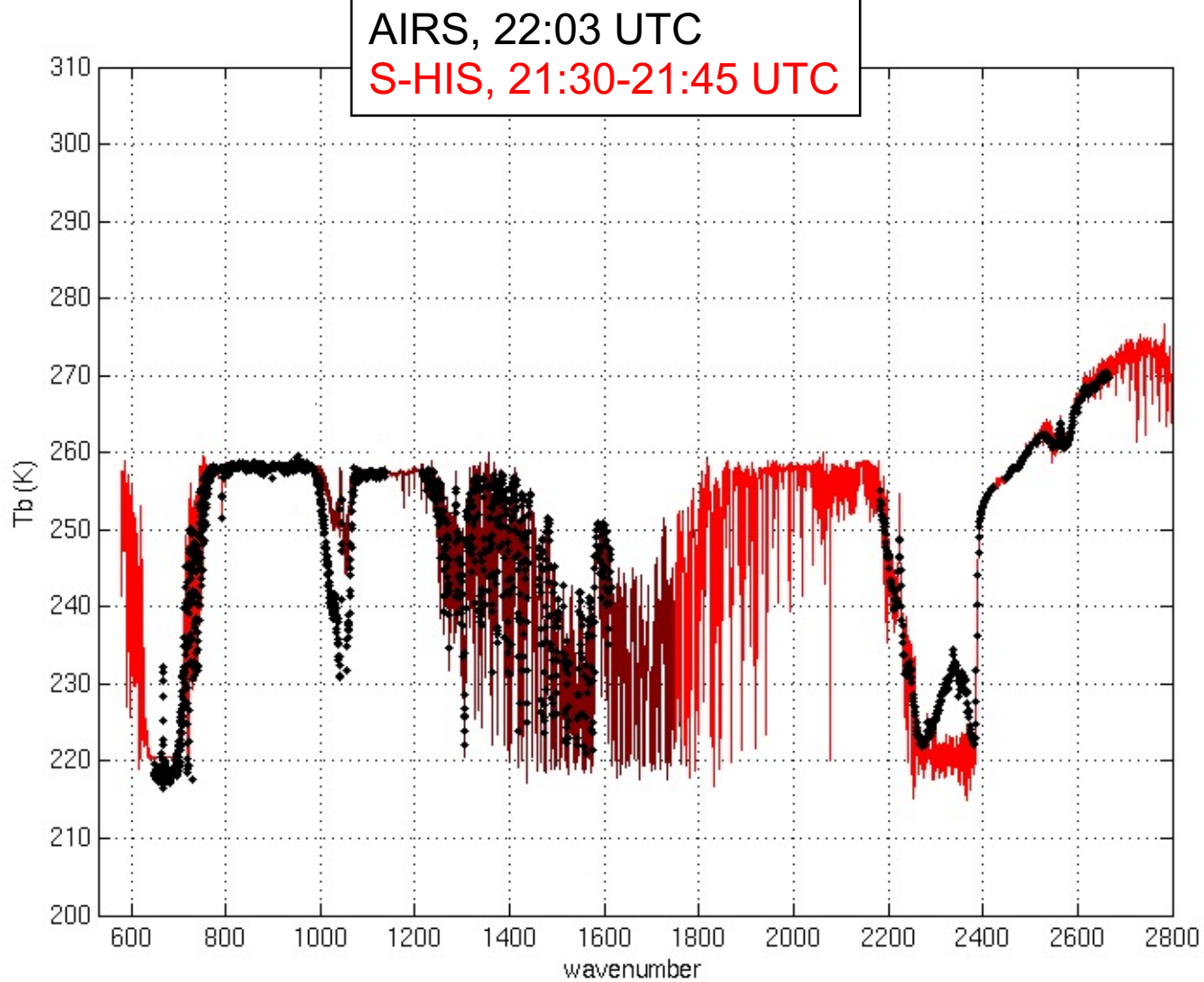
MPACE 10/09



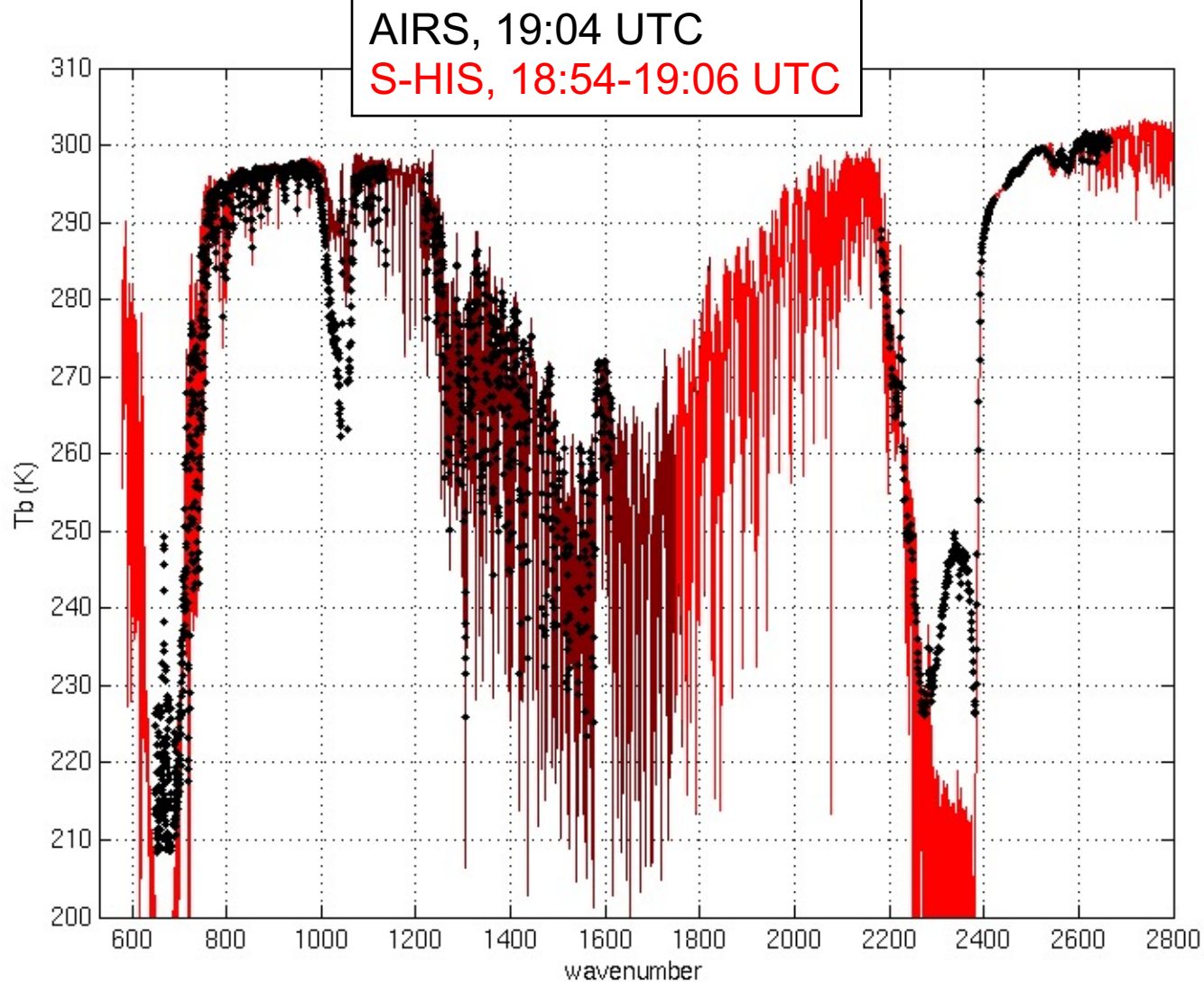
MPACE 10/09



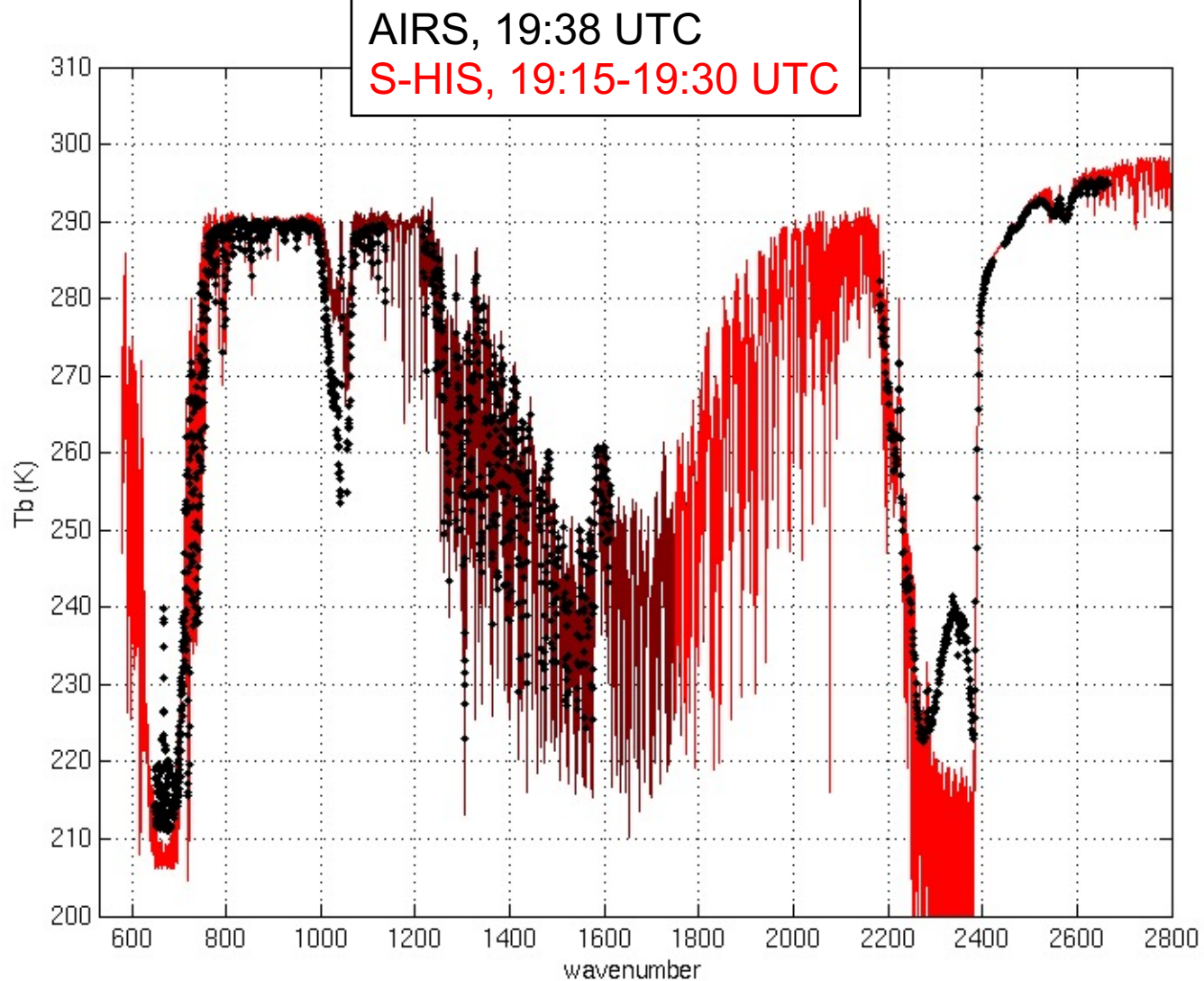
MPACE 10/12



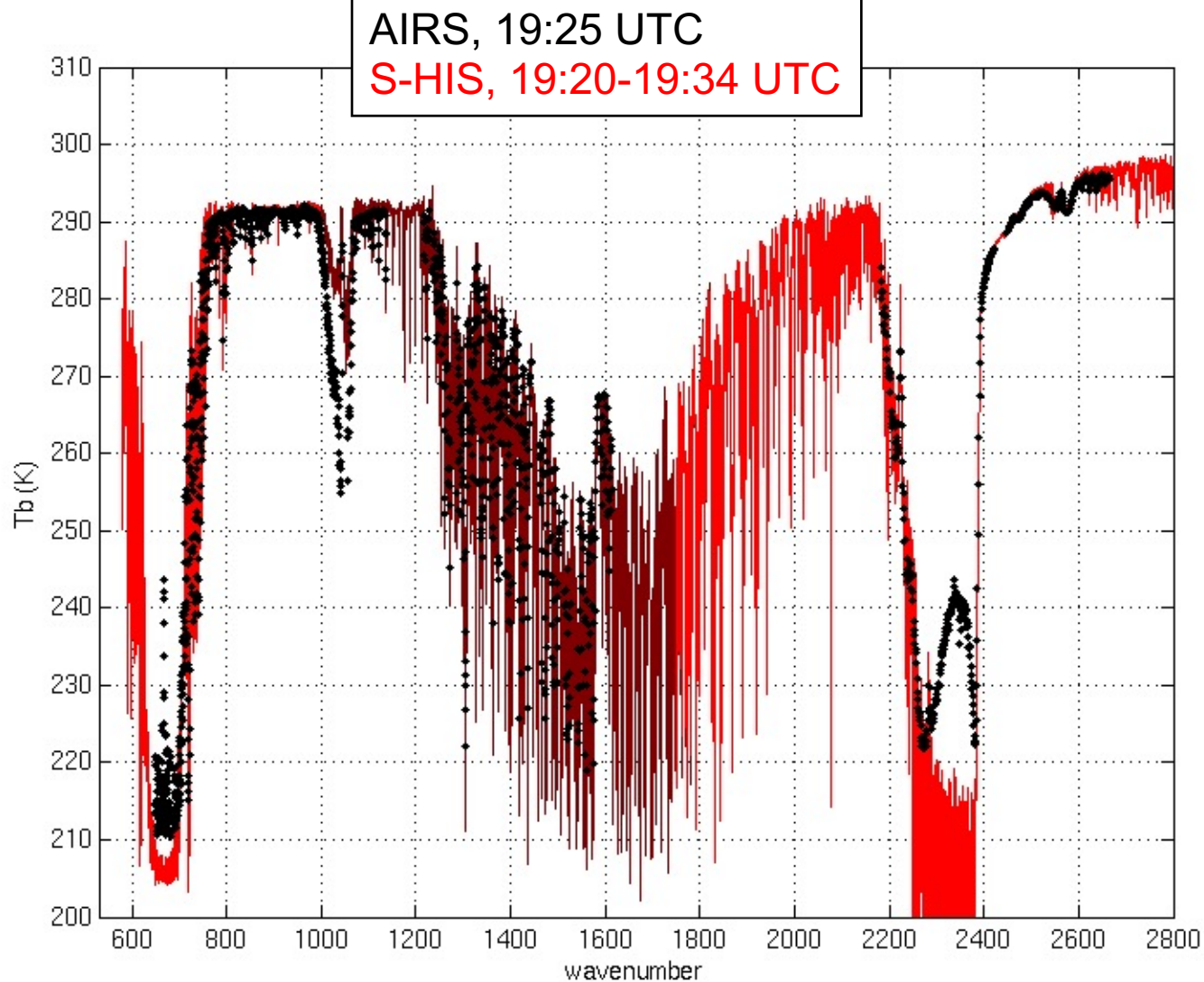
AVE Flight 10/31



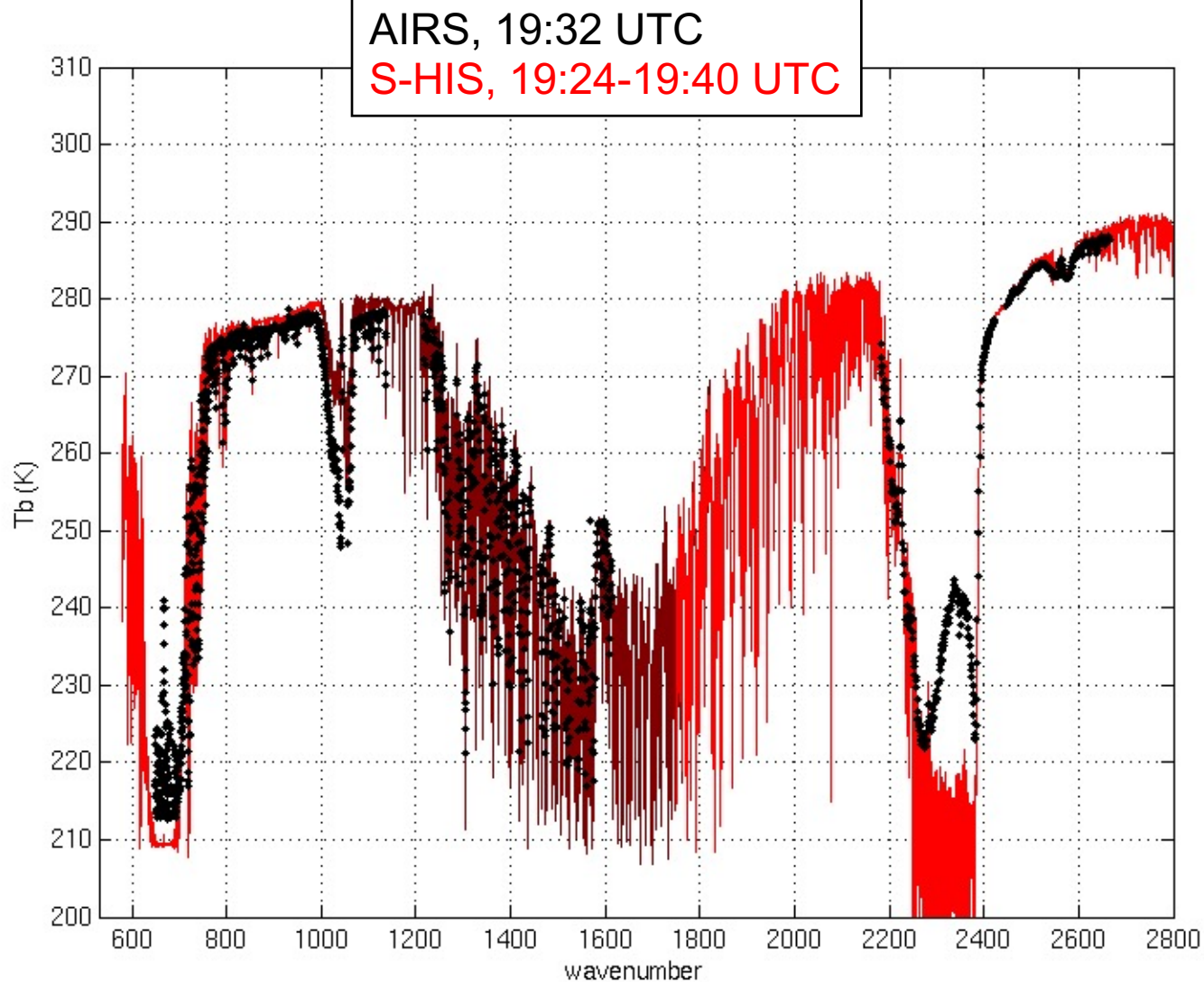
AVE Flight 11/03



AVE Flight 11/05



AVE Flight 11/12





4. The Promise of CrlS **for NPOESS**

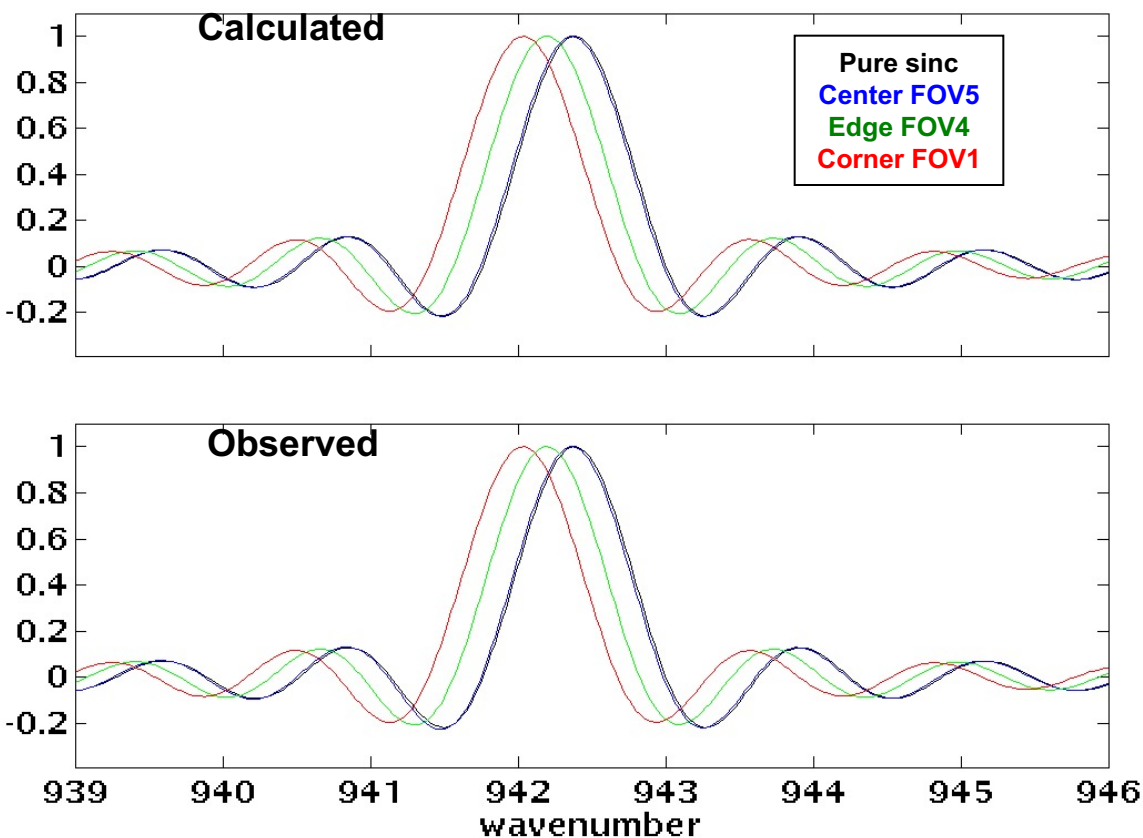
CrIS, AIRS Successor for NPOESS will be even better

- 1. Radiometric Calibration: < 0.4 K 3-sigma
(Design specs: < 0.45%, LW, 0.58% MW, 0.77% SW)**
- 2. Spectral Calibration:
Instrument Line Shape (ILS) extremely well
known and stable from first principles**
- 3. Noise:
4x smaller than AIRS in the LW CO₂ region**

CrIS Observed and Calculated Instrument Line Shape (ILS)

CO₂ laser source, Center, Edge & Corner Pixels of 3x3 array

($\lambda_{\text{laser}} = 775.18765 \text{ nm}$, $\nu_{\text{CO}_2\text{laser}} = 942.383333 \text{ cm}^{-1}$, $dx = -0.7 \text{ mrad}$, $dy = 0.1 \text{ mrad}$)

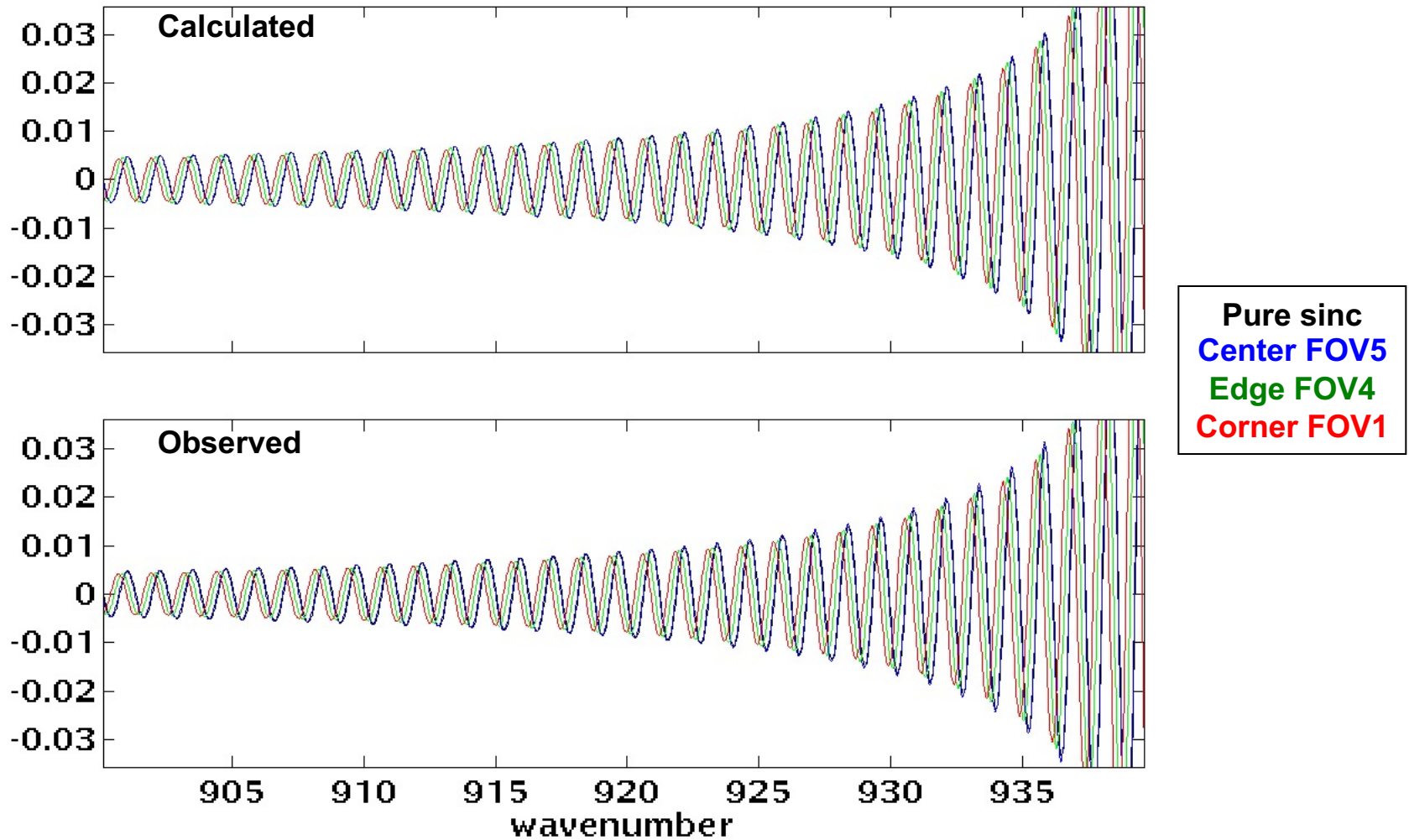


		Center FOV	Edge FOV	Corner FOV
centroid (cm ⁻¹)	Obs	942.367	942.195	942.034
	Calc	942.366	942.195	942.034
FWHM (cm ⁻¹)	Obs	0.747	0.757	0.767
	Calc	0.751	0.759	0.767
Lfoot	Obs	0.358	0.329	0.313
	Calc	0.347	0.328	0.313
Rfoot	Obs	0.347	0.326	0.311
	Calc	0.345	0.329	0.313

FTS design expectations confirmed

Observed and Calculated ILSs for Run1, FOVs 5, 4, and 1

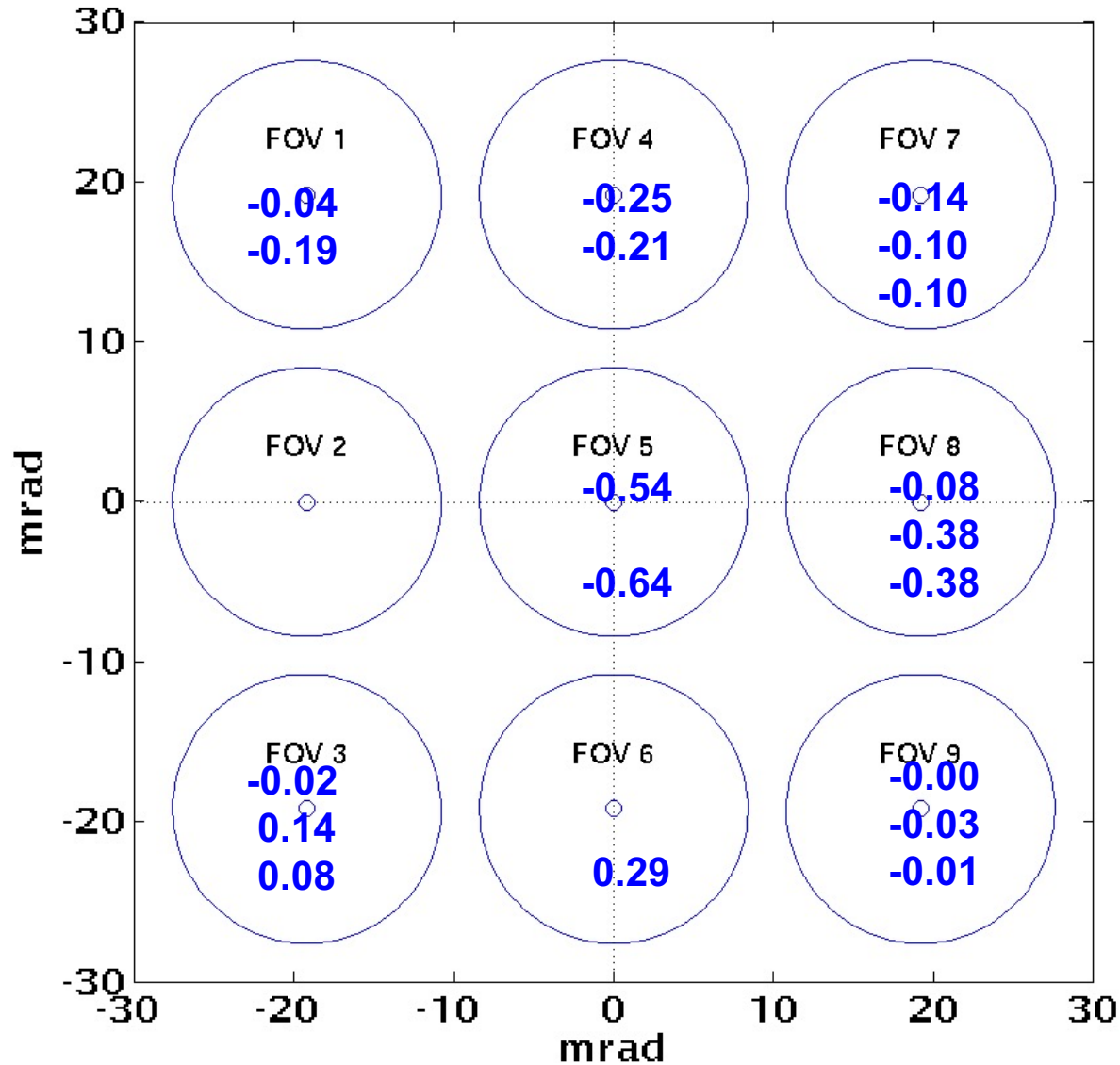
$$\lambda_{\text{laser}} = 775.18765 \text{ nm}, \nu_{\text{CO}_2\text{laser}} = 942.383333 \text{ cm}^{-1}, dx = -0.7 \text{ mrad}, dy = 0.1 \text{ mrad}$$



CrIS ILS Quantitative Verification

Δ width (%) for all FOVs

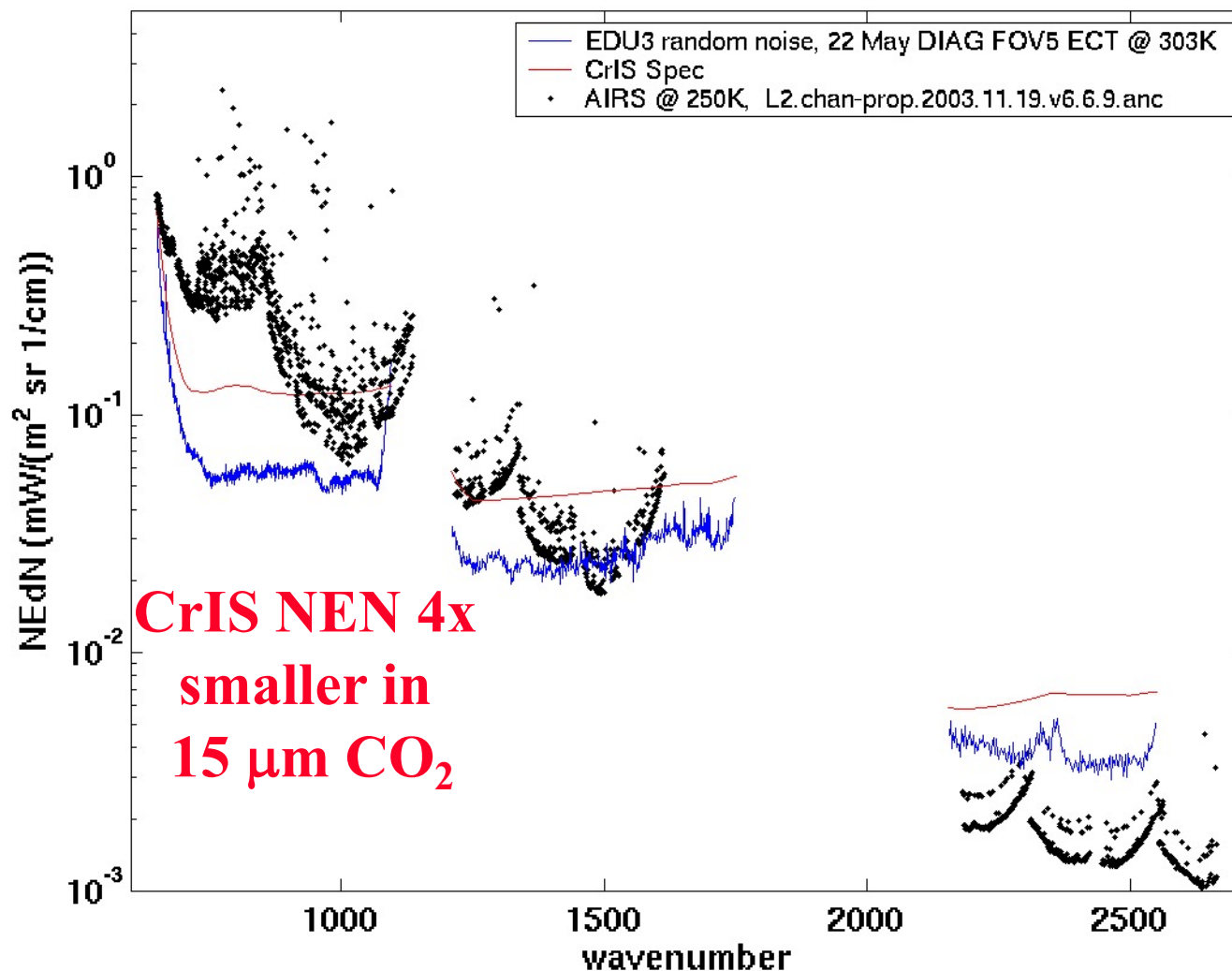
with small overall array shift $dx = -0.7$ mrad, $dy = 0.1$ mrad



Normal Spec

Δ width < 1%

NEN Comparion with AIRS (AIRS, CrIS random, CrIS Spec)



AIRS for 250K scene, CrIS for 303 K (SW NENs similar for 300K scene)

**Calibration and Validation of
upwelling IR radiance observations
are now concerned with
tenths of K, not degrees K !**

**High Spectral Resolution is an
important part of the reason
(Goody & Haskins, J Climate, 1998)**